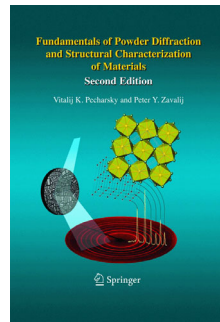
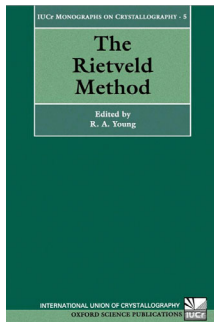
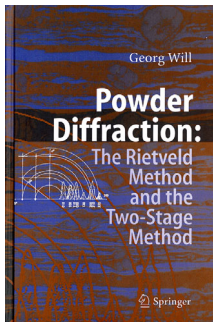
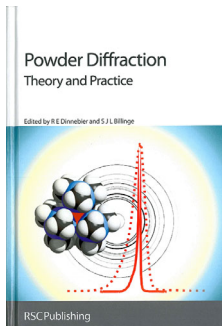
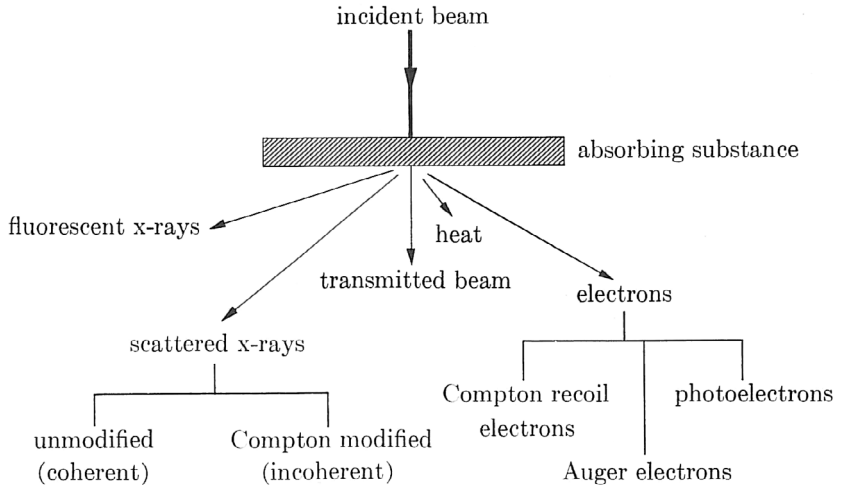


# X-ray powder diffraction – a practical guide

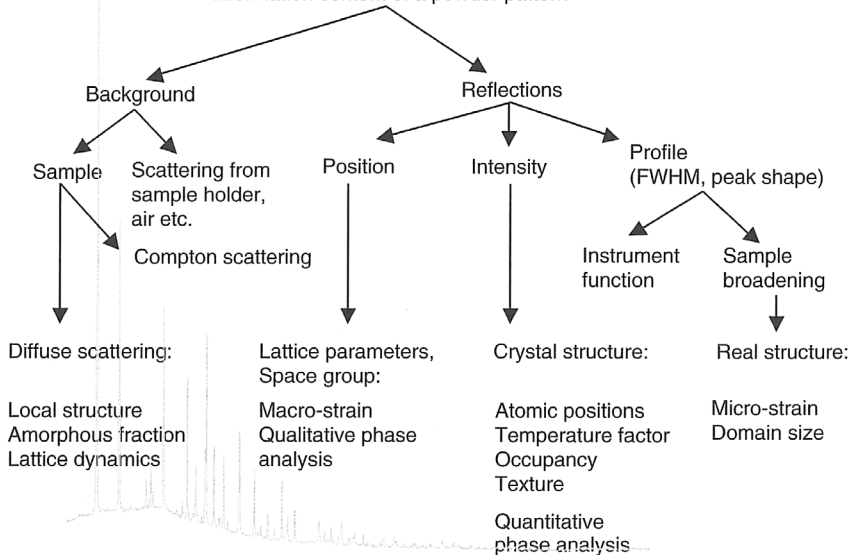


# X-ray hitting condensed matter



# X-ray hitting condensed matter

Information content of a powder pattern

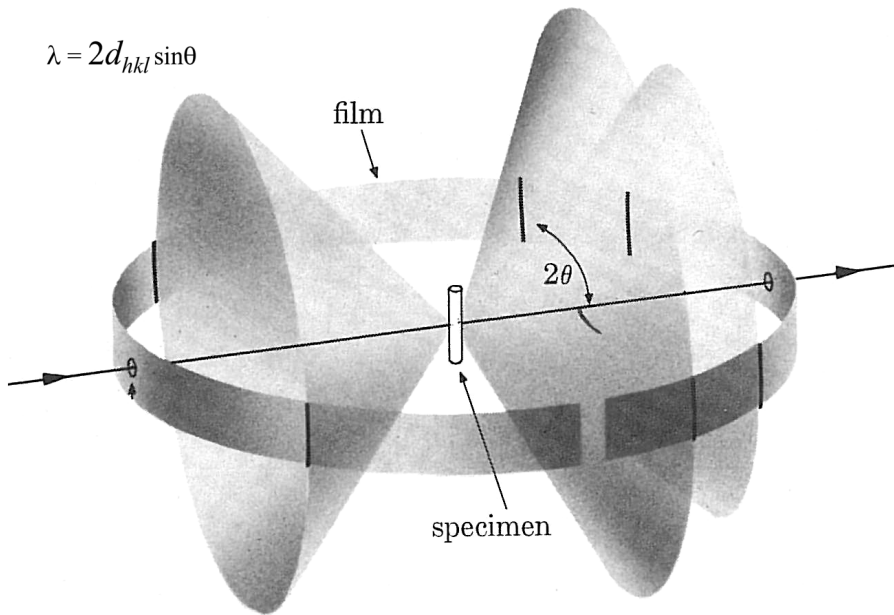


$$\lambda = 2d_{hkl} \sin \theta$$

$$\mathbf{F}(\mathbf{h}) = \sum_{j=1}^n g^j t^j(s) f^j(s) \exp(2\pi i \mathbf{h} \cdot \mathbf{x}^j)$$

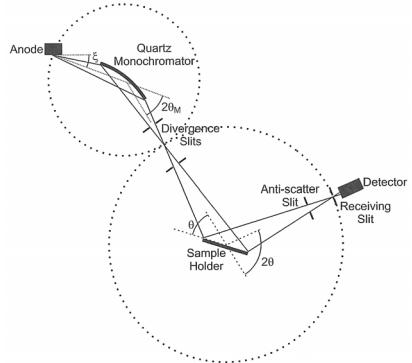
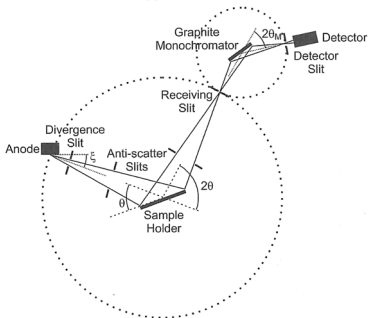
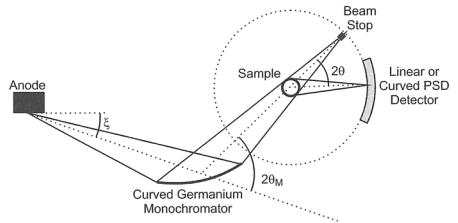
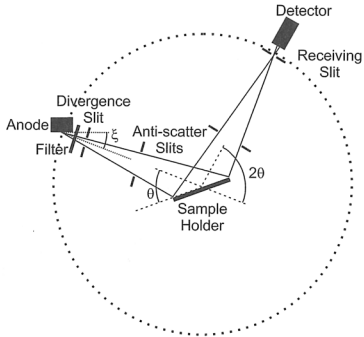
# Debye-Scherrer cones from a polycrystalline sample

$$\lambda = 2d_{hkl} \sin\theta$$

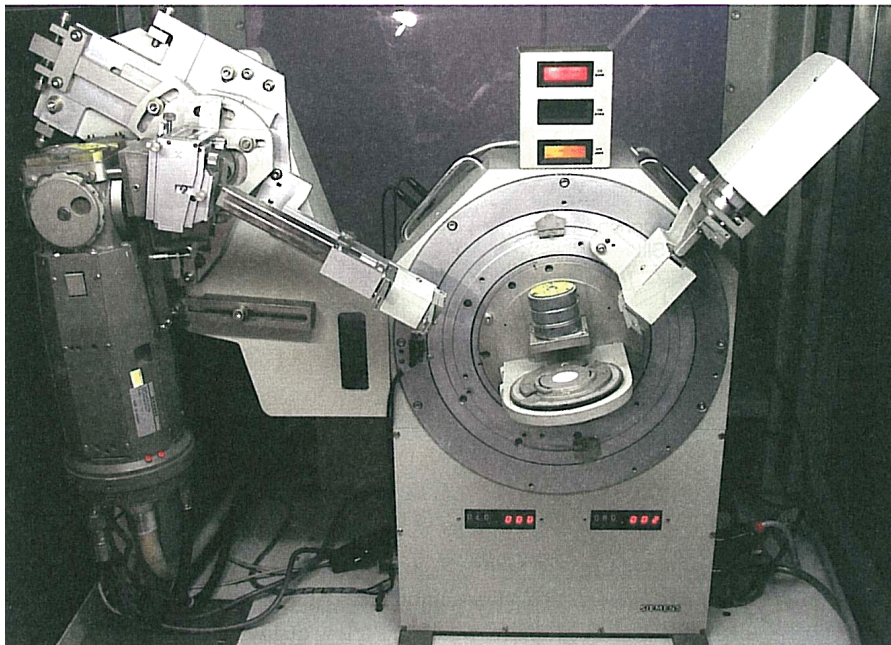




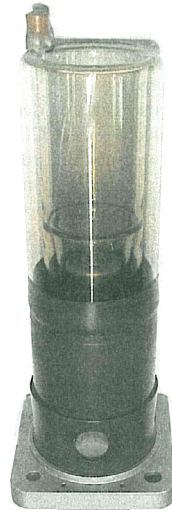
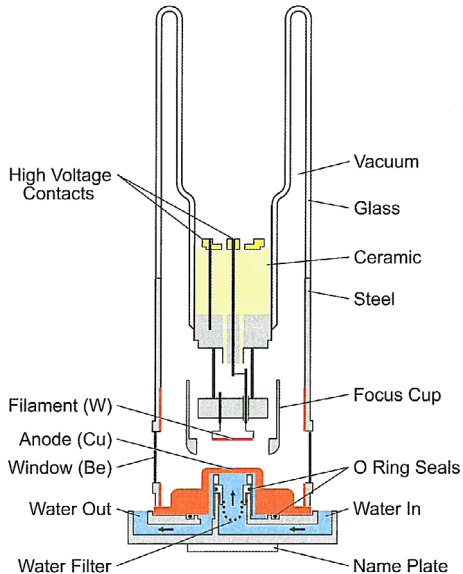
# Bragg-Brentano and Guinier diffractometer



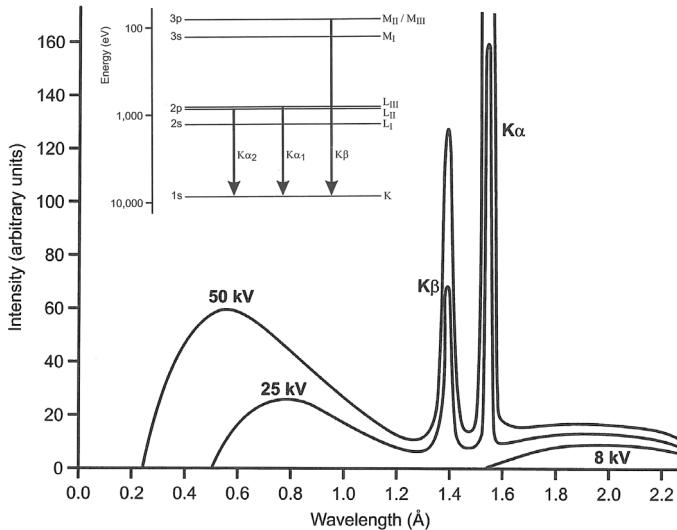
# Bragg-Brentano diffractometer with monochromator



# Generation of x-ray

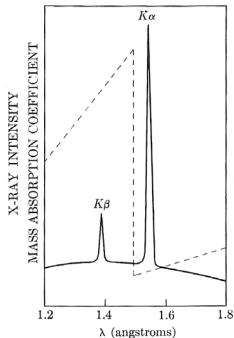


# Generation of x-ray

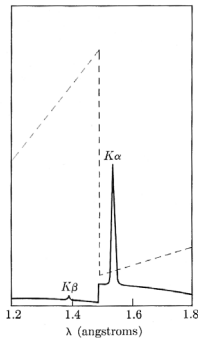


Optimum voltage  $\sim 4$  times characteristic energy ( $\sim 30$  kV for Cu anodes)

# Generation of x-ray



(a) No filter



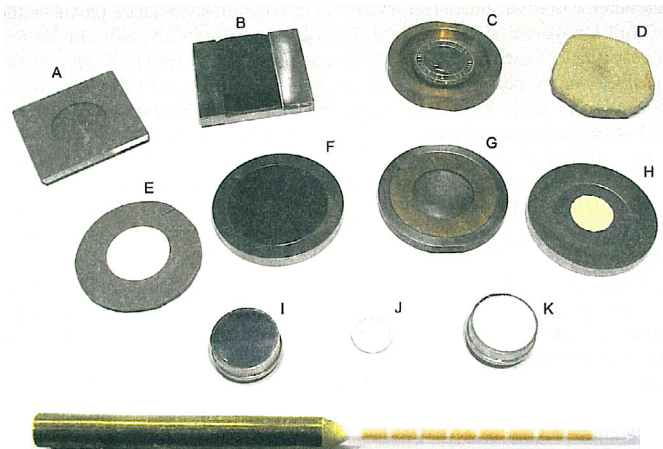
(b) Nickel filter

Target	Filter	Incident beam* $\frac{I(K\alpha)}{I(K\beta)}$	Filter thickness for $\frac{I(K\alpha)}{I(K\beta)} = \frac{500}{1}$ in trans. beam		$\frac{I(K\alpha) \text{ trans.}}{I(K\alpha) \text{ incident}}$
			mg/cm <sup>2</sup>	in.	
Mo	Zr	5.4	77	0.0046	0.29
Cu	Ni	7.5	18	0.0008	0.42
Co	Fe	9.4	14	0.0007	0.46
Fe	Mn	9.0	12	0.0007	0.48
Cr	V	8.5	10	0.0006	0.49

\* This is the intensity ratio *at the target* [G.11, Vol. 3, p. 71]. This ratio outside the x-ray tube will be changed somewhat by the differential absorption of K $\alpha$  and K $\beta$  by the tube window, typically beryllium, 0.01 inch (0.25 mm) thick.

Suppression of K $\beta$  radiation by filter with lighter neighbor element in periodic table

# Samples for x-ray powder diffraction



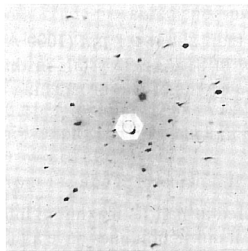
Well prepared samples at the right sample holder is the key for success!!!

## Samples for x-ray powder diffraction

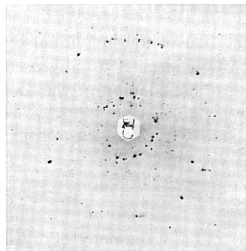


Hygiene in preparing the powder is the second key for success!!!

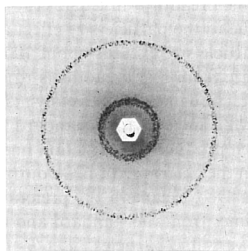
## Samples for x-ray powder diffraction



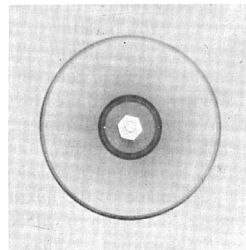
(a)



(b)



(c)

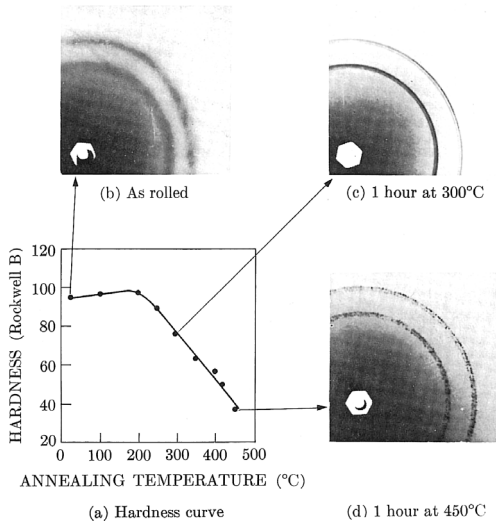


(d)

**Fig. 9-1** Back-reflection pinhole patterns of recrystallized aluminum specimens; grain size decreases in the order (a), (b), (c), (d). Filtered copper radiation.



# Samples for x-ray powder diffraction

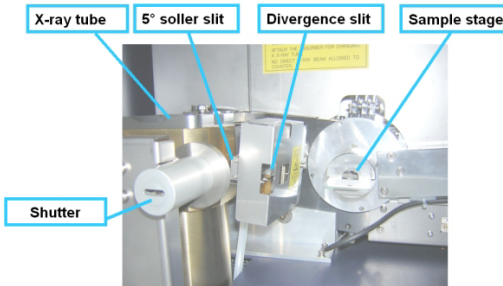


**Fig. 9-3** Changes in hardness and diffraction lines of 70 Cu-30 Zn specimens, reduced in thickness by 90 percent by cold rolling, and annealed for 1 hour at the temperatures indicated in (a). (b), (c), and (d) are portions of back-reflection pinhole patterns of specimens annealed at the temperatures stated (filtered copper radiation).

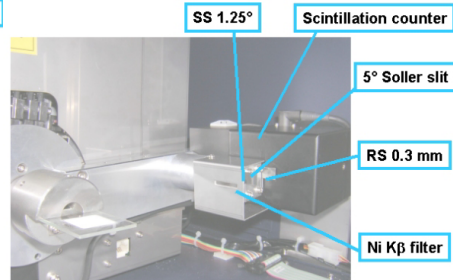
# Bragg-Brentano diffractometer for the desk



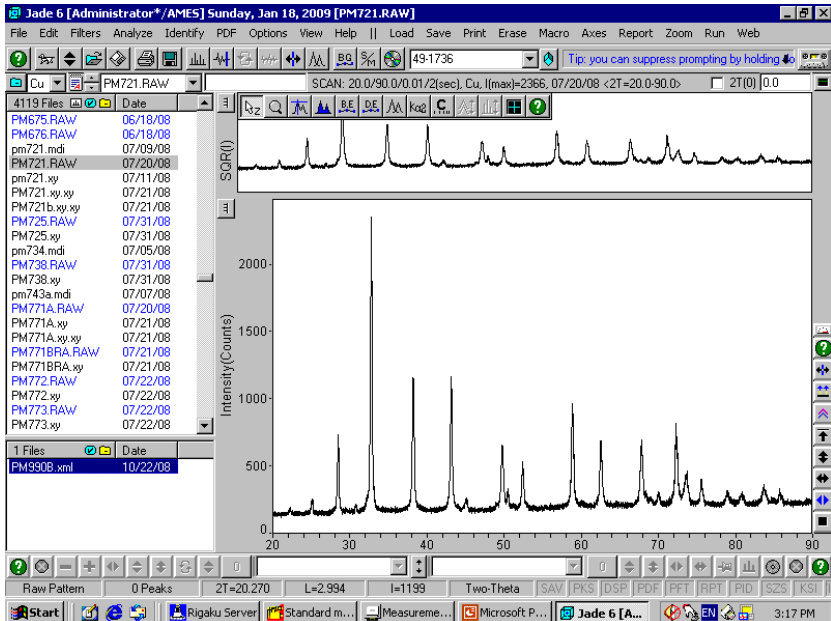
## Goniometer & optics (incident)



## Goniometer & optics (receiving)



# Example: growth of PrAuSi out of Sn flux



Which phases are present?

# Phase analysis with the PDF database

## POWDER DIFFRACTION FILE

### Sets 1-5 (Revised)

Inorganic Volume, No. PD1S-5iRB

Published by the  
JOINT COMMITTEE ON POWDER DIFFRACTION STANDARDS  
1601 Park Lane, Swarthmore, Pennsylvania 19081  
U.S.A.

33-1161

33-1162

d	3.34	4.26	1.82	4.26	SiO <sub>2</sub>	★
I/I <sub>1</sub>	100	22	14	22	Silicon Oxide	
Quartz, low						
Rad. CuKα; λ 1.540598 Filter Mono. Dia. Cutoff 1/1; Diffractometer I/I cor.						
Ref. Nat. Bur. Stand. (U.S.) Monogr. 25, Sec. 18 (1981)						
Sys. Hexagonal S.G. P3 <sub>2</sub> 1 (152)	d Å	I/I <sub>1</sub>	hkl	d Å	I/I <sub>1</sub>	hkl
a <sub>0</sub> 4.9133(2) <sub>b0</sub> c <sub>0</sub> 5.4053(4) Å C 1.1001	2.257	22	100	1.2285	1	320
α Ref. Ibid. β γ Z 3 D <sub>6</sub> 2.649	2.457	100	101	1.1999	2	213
	2.282	8	110	1.1978	1	221
	2.237	4	111	1.1804	3	310
	2.127	6	200	1.1532	1	311
	1.9792	4	201	1.1405	<1	204
	1.8179	14	112	1.1143	<1	303
	1.6021	<1	003	1.0813	2	312
	1.6719	4	202	1.0635	<1	400
±a nωβ 1.544 ±γ 1.553 Sign +	1.6591	2	103	1.0476	1	105
2V D 2.656 mp Color Colorless	1.6082	<1	210	1.0438	<1	401
Ref. Ibid.	1.5418	9	211	1.0347	<1	214
	1.4556	1	113	1.0150	1	223
	1.4189	<1	300	0.9898	1	402
	1.3820	6	212	0.9873	1	313
	1.3752	7	203	0.9783	<1	304
	1.3718	8	301	0.9752	1	320
	1.2880	2	104	0.9636	<1	205
	1.2558	2	302	6 reflections to 0.9089		

Sample from the Glass Section at the National Bureau of Standards; ground single crystals of optical quality, locality unknown. Pattern at 25°C.  
Silicon (a<sub>0</sub>=5.43088Å) used as internal standard.  
F<sub>1</sub> = 76.6(0.0126, 31). Quartz group.  
To replace 5-490.

### I-0024 MAJOR CORRECTION

0086 1-0224	12.8	3.80	6.9	12.8	ZnOCl <sub>2</sub> ·8H <sub>2</sub> O					
1/I <sub>1</sub> 1-0224	100	83	67	100	ZIRCONIUM OXYCHLORIDE OCTA HYDRATE					
Rad. MoKα	λ 0.709		Filter ZnO <sub>2</sub>	d Å	I/I <sub>1</sub>	hkl	d Å	I/I <sub>1</sub>	hkl	
Dia. 16 INCHES Cut off			Coll.	12.8	100	100	2.07	13		
I/I <sub>1</sub> CALIBRATED STRIPS			d corr. abs.?	10.6	27	001	2.00	7		
Ref. H			No	7.9	20	101	1.91	13		
				6.9	67	111	1.81	13		
				4.80	13	102	1.71	13		
Sys. TETRAGONAL	S.G.			4.12	27	221	1.62	13		
a 12.9 b c. 10.6 A	C			3.82	20	212, 311	1.57	7		
α β γ	Z			3.60	83	320	1.51	7		
Ref. B.P. (COMPUTED FROM POWDER DATA)				3.24	40	400	1.46	7		
				2.96	7	213	1.42	7		
Fe	nμβ 1.5521 γ 1.563		Sign +	2.74	7	402				
2V	D			2.55	7	430, 104				
Ref. Wa	mp Color			2.39	7	520				
				2.22	13	304, 441				
				2.15	20	600				
						INDEXED BY B.P.				

### I-0378 MAJOR CORRECTION

d	4.30	3.81	4.08	4.30	SiO <sub>2</sub>	SiO <sub>2</sub>
I/I <sub>1</sub>	100	67	33	100	SILICON DIOXIDE	TRIDYMITE (LOW FORM)
Rad. MoKα λ 0.709 Filter ZnO <sub>2</sub>	d Å	I/I <sub>1</sub>	hkl	d Å	I/I <sub>1</sub>	hkl
Dia. 16 INCHES Cut off Coll. d corr. abs.?	4.30	100		1.44	3	
I/I <sub>1</sub> CALIBRATED STRIPS	4.08	33		1.40	7	
Ref. H <sub>1</sub>	3.81	67		1.36	3	
	3.43	1		1.31	4	
	3.21	1		1.25	3	
Sys. ORTHORHOMBIC S.G. C 0.954	2.96	17		1.19	5	
a 9.88 b 17.1 c 16.3 A 578 ° C 64 °	2.80	3		1.15	3	
Ref. WY (FOR ONLY ONE TYPE OF TRIDYMITE)	2.49	27		1.10	1	
	2.31	11				
±a 1.478 nωβ 1.479 γ 1.481 Sign +	2.08	5				
2V 35° D 2.26 mp Color COLORLESS	1.84	3				
Ref. Wn, C.C. (FOR ONLY ONE TYPE OF TRIDYMITE)	1.69	8				
	1.64	4				
	1.60	4				
	1.53	5				
T.P. TO β <sub>1</sub> (LOWER HIGH-TRIDYMITE) AT 117°C						
T.P. TO β <sub>2</sub> (UPPER HIGH-TRIDYMITE) AT 163°C						
SPECIMEN WAS HARD REFRACTORY BRICK						
LOW TRIDYMITE OCCURS IN MANY POLYTYPE FORMS, THE PATTERNS OF WHICH ARE CHARACTERIZED BY THE SAME STRONG REFLECTIONS AND DIFFERENT WEAK ONES (SEE ALSO OTHER TRIDYMITE CARDS). SEE FLORE, BR., DEUT. KERAM. GZ. 32, 362-52 (1955) FOR REPRODUCTIONS OF X-RAY PHOTOGRAPHS.						



# Phase analysis with the PDF database

## Powder Diffraction File Search Manual

### Hanawalt Method

### Inorganic

1987



Published by the

INTERNATIONAL CENTRE FOR DIFFRACTION DATA

1601 PARK LANE • SWARTHMORE, PA 19081-2389 • U.S.A.

### FINK

## POWDER DIFFRACTION FILE

## RETRIEVAL INDEX

for

## INORGANIC COMPOUNDS

1972

Publication PDIS-22f

Published by the

JOINT COMMITTEE ON POWDER DIFFRACTION STANDARDS

1601 Park Lane, Swarthmore, Pennsylvania 19081

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File No.

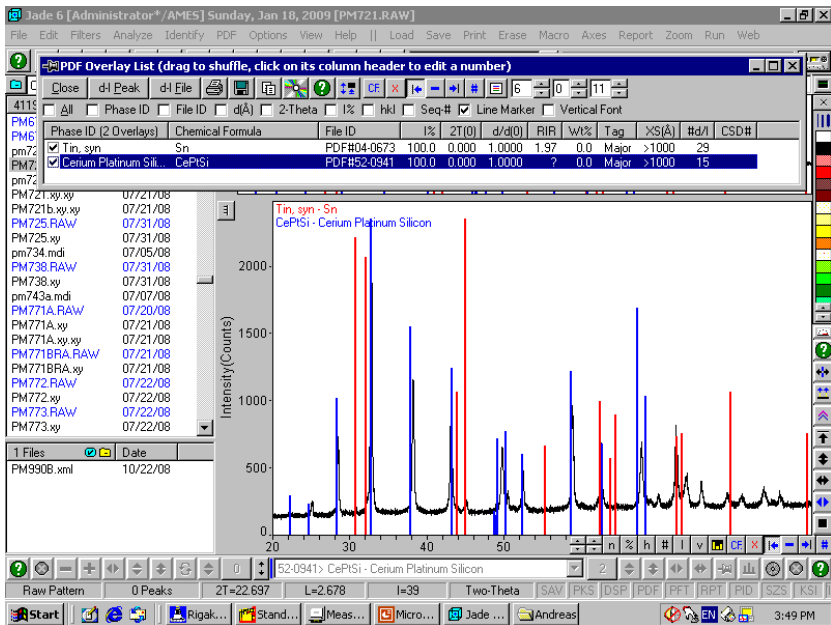
10.6 <sub>x</sub>	44.0 <sub>x</sub>	21.8 <sub>x</sub>	3.19 <sub>x</sub>	4.87 <sub>x</sub>	14.3 <sub>x</sub>	3.33 <sub>x</sub>	1.97 <sub>x</sub>	NaKA <sub>2</sub> (Si <sub>3</sub> Al) <sub>3</sub> O <sub>10</sub> (OH) <sub>2</sub> ·2H <sub>2</sub> O/Torcasovite	26- 970
14.1 <sub>x</sub>	28.0 <sub>x</sub>	2.98 <sub>x</sub>	2.70 <sub>x</sub>	4.85 <sub>x</sub>	4.44 <sub>x</sub>	5.27 <sub>x</sub>	5.60 <sub>x</sub>	CoCu <sub>2</sub> (AsO <sub>4</sub> ) <sub>2</sub> (CO <sub>3</sub> )(OH) <sub>2</sub> ·6H <sub>2</sub> O/Tyrolite	11- 348
8.04 <sub>x</sub>	24.1 <sub>x</sub>	3.44 <sub>x</sub>	3.02 <sub>x</sub>	2.68 <sub>x</sub>	1.61 <sub>x</sub>	1.78 <sub>x</sub>	2.41 <sub>x</sub>	Na <sub>3</sub> Bo <sub>3</sub> NbSi <sub>3</sub> O <sub>10</sub> (F,OH)·Na <sub>2</sub> PO <sub>3</sub> /Bornemanite	29-1176
11.9 <sub>x</sub>	23.1 <sub>x</sub>	9.10 <sub>x</sub>	3.18 <sub>x</sub>	6.91 <sub>x</sub>	13.9 <sub>x</sub>	9.70 <sub>x</sub>	8.00 <sub>x</sub>	Fe <sub>4</sub> (PO <sub>4</sub> ) <sub>3</sub> (OH) <sub>2</sub> ·12H <sub>2</sub> O/Cocconite	14- 331
11.0 <sub>x</sub>	22.0 <sub>x</sub>	3.12 <sub>x</sub>	4.20 <sub>x</sub>	1.82 <sub>x</sub>	3.65 <sub>x</sub>	2.80 <sub>x</sub>	8.40 <sub>x</sub>	Ca <sub>2</sub> (Si <sub>3</sub> O <sub>13</sub> )(OH) <sub>2</sub> ·3H <sub>2</sub> O/Gyrolite	9- 449
i 11.7 <sub>x</sub>	21.0 <sub>x</sub>	4.12 <sub>x</sub>	1.40 <sub>x</sub>	7.80 <sub>x</sub>	3.75 <sub>x</sub>	2.32 <sub>x</sub>	5.70 <sub>x</sub>	Al <sub>2</sub> Si <sub>2</sub> O <sub>7</sub> (OH) <sub>2</sub> ·xH <sub>2</sub> O/Imogolite	25-1493
i 8.84 <sub>x</sub>	21.0 <sub>x</sub>	1.82 <sub>x</sub>	2.95 <sub>x</sub>	2.92 <sub>x</sub>	3.11 <sub>x</sub>	3.00 <sub>x</sub>	2.80 <sub>x</sub>	CoSi <sub>2</sub> O <sub>7</sub> ·2H <sub>2</sub> O/Okenite	33- 305
i 8.97 <sub>x</sub>	18.7 <sub>x</sub>	2.86 <sub>x</sub>	3.13 <sub>x</sub>	9.46 <sub>x</sub>	4.79 <sub>x</sub>	4.21 <sub>x</sub>	3.35 <sub>x</sub>	Cu <sub>2</sub> (AsO <sub>4</sub> )(OH) <sub>2</sub> ·5H <sub>2</sub> O/Strohmilchite	21- 289
i 9.29 <sub>x</sub>	18.4 <sub>x</sub>	5.57 <sub>x</sub>	6.15 <sub>x</sub>	3.58 <sub>x</sub>	3.49 <sub>x</sub>	4.70 <sub>x</sub>	5.32 <sub>x</sub>	Fe <sub>2</sub> O <sub>3</sub> (SO <sub>4</sub> ) <sub>1/2</sub> ·63H <sub>2</sub> O/Copiapite	35- 583
i 9.08 <sub>x</sub>	18.2 <sub>x</sub>	2.02 <sub>x</sub>	3.29 <sub>x</sub>	2.90 <sub>x</sub>	3.76 <sub>x</sub>	3.07 <sub>x</sub>	2.60 <sub>x</sub>	Na <sub>2</sub> K <sub>2</sub> Fe <sub>2</sub> (SO <sub>4</sub> ) <sub>2</sub> O <sub>2</sub> ·18H <sub>2</sub> O/Metavoltine	29-1043
o 9.20 <sub>x</sub>	18.1 <sub>x</sub>	5.58 <sub>x</sub>	6.17 <sub>x</sub>	3.58 <sub>x</sub>	3.50 <sub>x</sub>	5.32 <sub>x</sub>	4.68 <sub>x</sub>	(Mg,Al)(Fe,Al)(SO <sub>4</sub> ) <sub>2</sub> (OH) <sub>2</sub> ·20H <sub>2</sub> O/Aluminocopi	20- 659
o 8.94 <sub>x</sub>	17.7 <sub>x</sub>	2.84 <sub>x</sub>	5.57 <sub>x</sub>	2.96 <sub>x</sub>	2.68 <sub>x</sub>	1.71 <sub>x</sub>	3.85 <sub>x</sub>	K <sub>2</sub> Na <sub>2</sub> Ca <sub>2</sub> Al <sub>2</sub> (PO <sub>4</sub> ) <sub>2</sub> (OH) <sub>2</sub> ·26H <sub>2</sub> O/Engelshite	29-1037
o 8.65 <sub>x</sub>	17.6 <sub>x</sub>	3.33 <sub>x</sub>	7.85 <sub>x</sub>	12.2 <sub>x</sub>	7.44 <sub>x</sub>	2.37 <sub>x</sub>	4.25 <sub>x</sub>	(Al,Fe) <sub>2</sub> AuO <sub>4</sub> (OH) <sub>2</sub> ·5H <sub>2</sub> O/Liskeardite	11- 146
i 15.1 <sub>x</sub>	17.0 <sub>x</sub>	11.3 <sub>x</sub>	12.2 <sub>x</sub>	11.1 <sub>x</sub>	8.57 <sub>x</sub>	5.98 <sub>x</sub>	9.80 <sub>x</sub>	HR(OH) <sub>2</sub> SO <sub>4</sub> ·2H <sub>2</sub> O	21- 361
i 12.2 <sub>x</sub>	17.0 <sub>x</sub>	11.3 <sub>x</sub>	15.1 <sub>x</sub>	11.1 <sub>x</sub>	8.57 <sub>x</sub>	5.98 <sub>x</sub>	9.80 <sub>x</sub>	HR(OH) <sub>2</sub> SO <sub>4</sub> ·2H <sub>2</sub> O	21- 361

10.0 and over

File No. Fiche No.

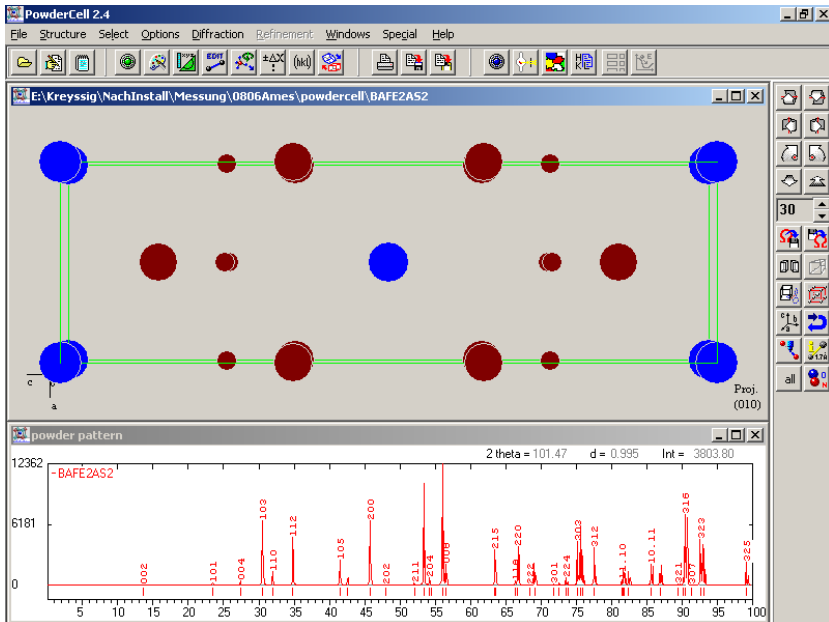
30.4 <sub>x</sub>	15.2 <sub>x</sub>	10.0 <sub>x</sub>	5.01 <sub>x</sub>	4.48 <sub>x</sub>	3.30 <sub>x</sub>	2.56 <sub>x</sub>	1.49 <sub>x</sub>	Al-Fe-Hg-Ca-Na-F-Si-O-H <sub>2</sub> O	22- 956 I-153-F 3
* 17.0 <sub>x</sub>	15.1 <sub>x</sub>	12.2 <sub>x</sub>	11.3 <sub>x</sub>	11.1 <sub>x</sub>	9.80 <sub>x</sub>	8.57 <sub>x</sub>	5.98 <sub>x</sub>	Bz(OH) <sub>2</sub> SO <sub>4</sub> ·2H <sub>2</sub> O	21- 361 I-134-C 3
30.0 <sub>x</sub>	15.0 <sub>x</sub>	4.97 <sub>x</sub>	4.53 <sub>x</sub>	3.29 <sub>x</sub>	2.98 <sub>x</sub>	2.54 <sub>x</sub>	1.51 <sub>x</sub>	Na-K-Ca-Hg-Al-Si-O-OH-H <sub>2</sub> O	12- 231 I- 46-B 5
29.2 <sub>x</sub>	14.6 <sub>x</sub>	9.70 <sub>x</sub>	7.38 <sub>x</sub>	4.90 <sub>x</sub>	3.63 <sub>x</sub>	3.27 <sub>x</sub>	2.92 <sub>x</sub>	Hg <sub>2</sub> Al <sub>2</sub> Si <sub>2</sub> O <sub>7</sub> (OH) <sub>2</sub> ·4H <sub>2</sub> O	13- 190 I- 52-E 4
28.0 <sub>x</sub>	14.1 <sub>x</sub>	5.60 <sub>x</sub>	5.27 <sub>x</sub>	4.85 <sub>x</sub>	4.44 <sub>x</sub>	2.98 <sub>x</sub>	2.70 <sub>x</sub>	Ca <sub>2</sub> Co <sub>2</sub> (AsO <sub>4</sub> ) <sub>2</sub> ·(OH) <sub>2</sub> ·10H <sub>2</sub> O	11- 345 I- 40-F 7
29.0 <sub>x</sub>	14.0 <sub>x</sub>	7.08 <sub>x</sub>	4.72 <sub>x</sub>	4.62 <sub>x</sub>	3.53 <sub>x</sub>	2.63 <sub>x</sub>	2.57 <sub>x</sub>	HgFeAlSi	19- 764 I-109-F 1
* 23.1 <sub>x</sub>	13.9 <sub>x</sub>	11.9 <sub>x</sub>	9.70 <sub>x</sub>	9.10 <sub>x</sub>	8.00 <sub>x</sub>	6.91 <sub>x</sub>	3.18 <sub>x</sub>	Fe <sub>2</sub> (PO <sub>4</sub> ) <sub>2</sub> (OH) <sub>2</sub> ·12H <sub>2</sub> O	18- 331 I- 59-B 6
* 16.1 <sub>x</sub>	13.8 <sub>x</sub>	10.6 <sub>x</sub>	9.07 <sub>x</sub>	7.12 <sub>x</sub>	4.82 <sub>x</sub>	4.72 <sub>x</sub>	3.83 <sub>x</sub>	C <sub>2</sub> H <sub>2</sub> N <sub>2</sub> O <sub>4</sub> ·0.3H <sub>2</sub> O	19- 69 I-103-2 2
o 14.5 <sub>x</sub>	12.9 <sub>x</sub>	11.8 <sub>x</sub>	7.20 <sub>x</sub>	4.88 <sub>x</sub>	4.25 <sub>x</sub>	2.60 <sub>x</sub>	0.00 <sub>x</sub>	ReGa <sub>2</sub> O <sub>6</sub>	21-1114 I-141-B 3
25.8 <sub>x</sub>	12.4 <sub>x</sub>	4.95 <sub>x</sub>	4.47 <sub>x</sub>	4.30 <sub>x</sub>	3.33 <sub>x</sub>	2.56 <sub>x</sub>	1.49 <sub>x</sub>	Al-Tl-Fe-K-Na-Si-OH	7- 330 I- 26-C 3
25.5 <sub>x</sub>	12.4 <sub>x</sub>	8.20 <sub>x</sub>	6.15 <sub>x</sub>	4.92 <sub>x</sub>	4.11 <sub>x</sub>	3.53 <sub>x</sub>	3.09 <sub>x</sub>	K-Hg-Fe-Al-Si-O-OH	13- 233 I- 53-B 3
24.7 <sub>x</sub>	12.4 <sub>x</sub>	4.94 <sub>x</sub>	3.54 <sub>x</sub>	3.10 <sub>x</sub>	2.48 <sub>x</sub>	2.05 <sub>x</sub>	1.90 <sub>x</sub>	Na-Ca-K-H <sub>2</sub> O-Al-Si-O-R·3H <sub>2</sub> O	14- 183 I- 57-12 2
o 17.6 <sub>x</sub>	12.2 <sub>x</sub>	8.65 <sub>x</sub>	7.95 <sub>x</sub>	7.44 <sub>x</sub>	4.25 <sub>x</sub>	3.33 <sub>x</sub>	2.37 <sub>x</sub>	(Al,Fe) <sub>2</sub> AsO <sub>4</sub> (OH) <sub>2</sub> ·5H <sub>2</sub> O	11- 146 I- 39-B 11
* 15.1 <sub>x</sub>	12.2 <sub>x</sub>	11.3 <sub>x</sub>	11.1 <sub>x</sub>	9.80 <sub>x</sub>	8.57 <sub>x</sub>	5.98 <sub>x</sub>	17.0 <sub>x</sub>	Re(OH) <sub>2</sub> SO <sub>4</sub> ·2H <sub>2</sub> O	21- 361 I-134-C 3
17.4 <sub>x</sub>	12.1 <sub>x</sub>	10.6 <sub>x</sub>	5.79 <sub>x</sub>	4.35 <sub>x</sub>	3.53 <sub>x</sub>	2.90 <sub>x</sub>	2.12 <sub>x</sub>	V <sub>2</sub> O <sub>5</sub> ·3H <sub>2</sub> O	7- 332 I- 76-C 4

# Example: growth of PrAuSi out of Sn flux



If your phase is not in the database – search for isostructural compounds...

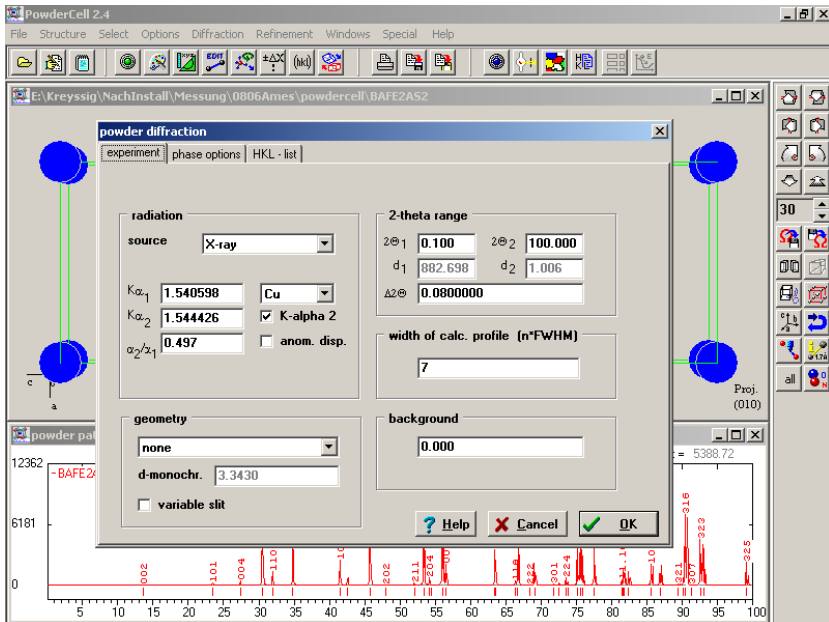
# Powdercell



The best tool to calculate diffraction pattern, to verify structure data and more...

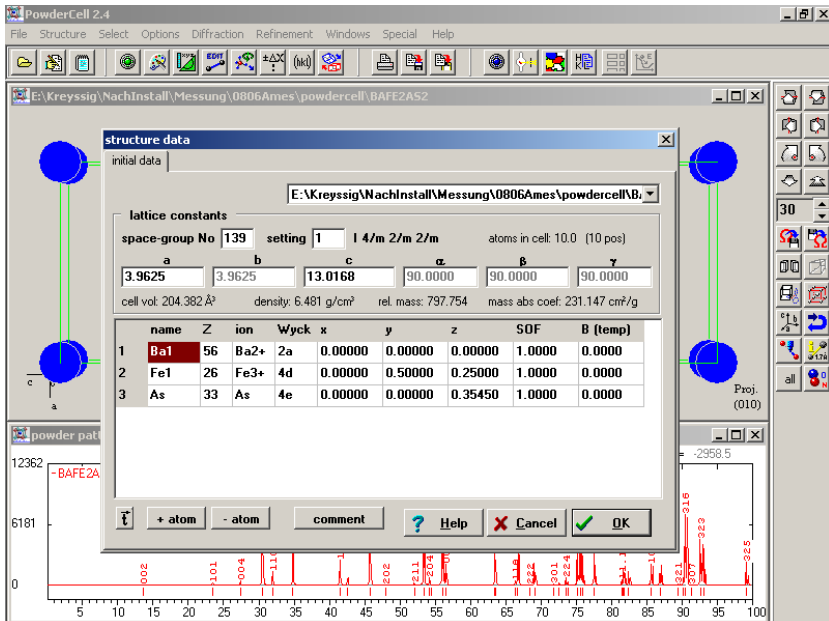


# Powdercell



The best tool to calculate diffraction pattern, to verify structure data and more...

# Powdercell



The best tool to calculate diffraction pattern, to verify structure data and more...

# International Tables for Crystallography

①  $Cmm2$

$C_{2v}^{11}$

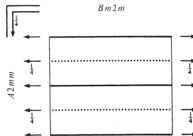
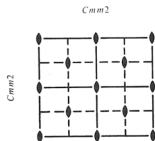
$mm2$

Orthorhombic

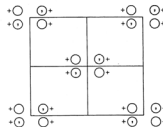
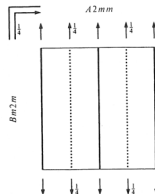
② No. 35

$Cmm2$

Patterson symmetry  $Cmmm$



③



④ Origin on  $mm2$

⑤ Asymmetric unit  $0 \leq x \leq \frac{1}{2}; 0 \leq y \leq \frac{1}{2}; 0 \leq z \leq 1$

⑥ Symmetry operations

For  $(0, 0, 0) +$  set

(1) 1

(2) 2  $0, 0, z$

(3)  $m$   $x, 0, z$

(4)  $m$   $0, y, z$

For  $(\frac{1}{2}, \frac{1}{2}, 0) +$  set

(1)  $i(\frac{1}{2}, \frac{1}{2}, 0)$

(2) 2  $\frac{1}{2}, \frac{1}{2}, z$

(3)  $a$   $x, \frac{1}{2}, z$

(4)  $b$   $\frac{1}{2}, y, z$

# International Tables for Crystallography

- ① *Headline:* Section 2.2.3.  
Short Hermann-Mauguin symbol  
(Section 2.2.4 and Chapter 12.2)      Schoenflies symbol  
(Chapters 12.1 and 12.2)      Crystal class (Point group)  
(Section 10.1.1 and Chapter 12.1)      Crystal system  
(Section 2.1.2)
- ② Number of space group  
[Same as in *IT* (1952)]      Full Hermann-Mauguin symbol  
(Section 2.2.4 and Chapter 12.3)      Patterson symmetry  
(Section 2.2.5)
- ③ *Space-group diagrams*, consisting of one or several projections of the symmetry elements and one illustration of a set of equivalent points in general position. The numbers and types of the diagrams depend on the crystal system. The diagrams and their axes are described in Section 2.2.6; the graphical symbols of symmetry elements are listed in Chapter 1.4.  
For monoclinic space groups see Section 2.2.16; for orthorhombic settings see Section 2.2.6.4.
- ④ *Origin* of the unit cell: Section 2.2.7. The site symmetry of the origin and its location with respect to the symmetry elements are given.
- ⑤ *Asymmetric unit*: Section 2.2.8. One choice of asymmetric unit is given.
- ⑥ *Symmetry operations*: Section 2.2.9 and Part 11. For each point  $\bar{x}, \bar{y}, \bar{z}$  of the general position that symmetry operation is listed which transforms the initial point  $x, y, z$  into the point under consideration. The symbol describes the nature of the operation, its glide or screw component (given between parentheses), if present, and the location of the corresponding symmetry element.  
The symmetry operations are numbered in the same way as the corresponding coordinate triplets of the general position. For centred space groups the same numbering is applied in each block, e.g. under 'For  $(\frac{1}{2}, \frac{1}{2}, 0)+$  set'.

[Continued on inside back cover]

# International Tables for Crystallography

## 1.4.1. Symmetry planes normal to the plane of projection (three dimensions) and symmetry lines in the plane of the figure (two dimensions)

Symmetry plane or symmetry line	Graphical symbol	Glide vector in units of lattice translation vectors parallel and normal to the projection plane	Printed symbol
Reflection plane, mirror plane Reflection line, mirror line (two dimensions)	—————	None	<i>m</i>
‘Axial’ glide plane Glide line (two dimensions)	-----	$\frac{1}{2}$ lattice vector along line in projection plane $\frac{1}{2}$ lattice vector along line in plane	<i>a</i> , <i>b</i> or <i>c</i> <i>g</i>
‘Axial’ glide plane	.....	$\frac{1}{2}$ lattice vector normal to projection plane	<i>a</i> , <i>b</i> or <i>c</i>
‘Double’ glide plane* (in centred cells only)	·····	Two glide vectors: $\frac{1}{2}$ along line parallel to projection plane, $\frac{1}{2}$ normal to projection plane	<i>e</i>
‘Diagonal’ glide plane	— · — · — · —	One glide vector with two components: $\frac{1}{2}$ along line parallel to projection plane, $\frac{1}{2}$ normal to projection plane	<i>n</i>
‘Diamond’ glide plane† (pair of planes; in centred cells only)	— · — · — · — — · — · — · —	$\frac{1}{4}$ along line parallel to projection plane, combined with $\frac{1}{4}$ normal to projection plane (arrow indicates direction parallel to the projection plane for which the normal component is positive)	<i>d</i>

\* For further explanations of the ‘double’ glide plane *e* see Note (iv) below and Note (x) in Chapter 1.3.

† See footnote § to Section 1.3.1.

# International Tables for Crystallography

## 1.4.2. Symmetry planes parallel to the plane of projection

Symmetry plane	Graphical symbol*	Glide vector in units of lattice translation vectors parallel to the projection plane	Printed symbol
Reflection plane, mirror plane		None	<i>m</i>
'Axial' glide plane		$\frac{1}{2}$ lattice vector in the direction of the arrow	<i>a</i> , <i>b</i> or <i>c</i>
'Double' glide plane† (in centred cells only)		Two glide vectors: $\frac{1}{2}$ in either of the directions of the two arrows	<i>e</i>
'Diagonal' glide plane		One glide vector with two components $\frac{1}{2}$ in the direction of the arrow	<i>n</i>
'Diamond' glide plane‡ (pair of planes; in centred cells only)		$\frac{1}{2}$ in the direction of the arrow; the glide vector is always half of a centring vector, i.e. one quarter of a diagonal of the conventional face-centred cell	<i>d</i>

\* The symbols are given at the upper left corner of the space-group diagrams. A fraction  $h$  attached to a symbol indicates two symmetry planes with 'heights'  $h$  and  $h + \frac{1}{2}$  above the plane of projection; e.g.  $\frac{1}{8}$  stands for  $h = \frac{1}{8}$  and  $\frac{5}{8}$ . No fraction means  $h = 0$  and  $\frac{1}{2}$  (cf. Section 2.2.6).

† For further explanations of the 'double' glide plane *e* see Note (iv) below and Note (x) in Chapter 1.3.

‡ See footnote § to Section 1.3.1.

# International Tables for Crystallography

## 1.4.5. Symmetry axes normal to the plane of projection and symmetry points in the plane of the figure

Symmetry axis or symmetry point	Graphical symbol*	Screw vector of a right-handed screw rotation in units of the shortest lattice translation vector parallel to the axis	Printed symbol (partial elements in parentheses)
Identity	None	None	1
Twofold rotation axis		None	2
Twofold rotation point (two dimensions) }		$\frac{1}{2}$	2 <sub>1</sub>
Twofold screw axis: '2 sub 1'		$\frac{1}{2}$	2 <sub>1</sub>
Threefold rotation axis		None	3
Threefold rotation point (two dimensions) }		$\frac{1}{3}$	3 <sub>1</sub>
Threefold screw axis: '3 sub 1'		$\frac{1}{3}$	3 <sub>1</sub>
Threefold screw axis: '3 sub 2'		$\frac{2}{3}$	3 <sub>2</sub>
Fourfold rotation axis		None	4 (2)
Fourfold rotation point (two dimensions) }		$\frac{1}{4}$	4 <sub>1</sub> (2 <sub>1</sub> )
Fourfold screw axis: '4 sub 1'		$\frac{1}{4}$	4 <sub>1</sub> (2 <sub>1</sub> )
Fourfold screw axis: '4 sub 2'		$\frac{1}{2}$	4 <sub>2</sub> (2)
Fourfold screw axis: '4 sub 3'		$\frac{3}{4}$	4 <sub>3</sub> (2 <sub>1</sub> )
Sixfold rotation axis		None	6 (3,2)
Sixfold rotation point (two dimensions) }		$\frac{1}{6}$	6 <sub>1</sub> (3 <sub>1</sub> , 2 <sub>1</sub> )
Sixfold screw axis: '6 sub 1'		$\frac{1}{6}$	6 <sub>1</sub> (3 <sub>1</sub> , 2 <sub>1</sub> )
Sixfold screw axis: '6 sub 2'		$\frac{1}{3}$	6 <sub>2</sub> (3 <sub>2</sub> , 2)
Sixfold screw axis: '6 sub 3'		$\frac{1}{2}$	6 <sub>3</sub> (3, 2 <sub>1</sub> )
Sixfold screw axis: '6 sub 4'		$\frac{2}{3}$	6 <sub>4</sub> (3 <sub>1</sub> , 2)
Sixfold screw axis: '6 sub 5'		$\frac{5}{6}$	6 <sub>5</sub> (3 <sub>2</sub> , 2 <sub>1</sub> )
Centre of symmetry, inversion centre: '1 bar'		None	$\bar{1}$
Reflection point, mirror point (one dimension) }		None	$\bar{1}$
Inversion axis: '3 bar'		None	$\bar{3}$ (3, $\bar{1}$ )
Inversion axis: '4 bar'		None	$\bar{4}$ (2)
Inversion axis: '6 bar'		None	$\bar{6} \equiv 3/m$
Twofold rotation axis with centre of symmetry		None	2/m ( $\bar{1}$ )
Twofold screw axis with centre of symmetry		$\frac{1}{2}$	2 <sub>1</sub> /m ( $\bar{1}$ )
Fourfold rotation axis with centre of symmetry		None	4/m ( $\bar{4}$ , 2, $\bar{1}$ )
'4 sub 2' screw axis with centre of symmetry		$\frac{1}{2}$	4 <sub>2</sub> /m ( $\bar{4}$ , 2, $\bar{1}$ )
Sixfold rotation axis with centre of symmetry		None	6/m ( $\bar{6}$ , $\bar{3}$ , 3, 2, $\bar{1}$ )
'6 sub 3' screw axis with centre of symmetry		$\frac{1}{2}$	6 <sub>3</sub> /m ( $\bar{6}$ , $\bar{3}$ , 3, 2, $\bar{1}$ )

\* Notes on the 'heights'  $h$  of symmetry points  $\bar{1}$ ,  $\bar{3}$ ,  $\bar{4}$  and  $\bar{6}$ :

- (1) Centres of symmetry  $\bar{1}$  and  $\bar{3}$ , as well as inversion points  $\bar{4}$  and  $\bar{6}$  on  $\bar{4}$  and  $\bar{6}$  axes parallel to  $[001]$ , occur in pairs at 'heights'  $h$  and  $h + \frac{1}{2}$ . In the space-group diagrams, only one fraction  $h$  is given, e.g.  $\frac{1}{2}$  stands for  $h = \frac{1}{2}$  and  $\frac{3}{2}$ . No fraction means  $h = 0$  and  $\frac{1}{2}$ . In cubic space groups, however, both fractions are given for vertical  $\bar{4}$  axes, including  $h = 0$  and  $\frac{1}{2}$ .
- (2) Symmetries  $4_1/m$  and  $6_1/m$  contain vertical  $\bar{4}$  and  $\bar{6}$  axes; their  $\bar{4}$  and  $\bar{6}$  inversion points coincide with the centres of symmetry. This is not indicated in the space-group diagrams.
- (3) Symmetries  $4_2/m$  and  $6_2/m$  also contain vertical  $\bar{4}$  and  $\bar{6}$  axes, but their  $\bar{4}$  and  $\bar{6}$  inversion points alternate with the centres of symmetry; i.e.  $\bar{1}$  points at  $h$  and  $h + \frac{1}{2}$  interleave with  $\bar{4}$  or  $\bar{6}$  points at  $h + \frac{1}{4}$  and  $h + \frac{3}{4}$ . In the tetragonal and hexagonal space-group diagrams, only one fraction for  $\bar{1}$  and one for  $\bar{4}$  or  $\bar{6}$  is given. In the cubic diagrams, all four fractions are listed for  $4_2/m$ ; e.g.  $Pn\bar{3}c$  (No. 223):  $\bar{1}$ : 0,  $\frac{1}{4}$ ,  $\frac{1}{2}$ ,  $\frac{3}{4}$ .

# International Tables for Crystallography

## 1.4.6. Symmetry axes parallel to the plane of projection

Symmetry axis	Graphical symbol*	Screw vector of a right-handed screw rotation in units of the shortest lattice translation vector parallel to the axis	Printed symbol (partial elements in parentheses)
Twofold rotation axis		None	2
Twofold screw axis: '2 sub 1'		$\frac{1}{2}$	2 <sub>1</sub>
Fourfold rotation axis		None	4 (2)
Fourfold screw axis: '4 sub 1'		$\frac{1}{4}$	4 <sub>1</sub> (2 <sub>1</sub> )
Fourfold screw axis: '4 sub 2'		$\frac{1}{2}$	4 <sub>2</sub> (2)
Fourfold screw axis: '4 sub 3'		$\frac{3}{4}$	4 <sub>3</sub> (2 <sub>1</sub> )
Inversion axis: '4 bar'		None	$\bar{4}$ (2)
Inversion point on '4 bar'-axis		—	$\bar{4}$ point

\* The symbols for horizontal symmetry axes are given outside the unit cell of the space-group diagrams. *Twofold* axes always occur in pairs, at 'heights'  $h$  and  $h + \frac{1}{2}$  above the plane of projection; here, a fraction  $h$  attached to such a symbol indicates two axes with heights  $h$  and  $h + \frac{1}{2}$ . No fraction stands for  $h = 0$  and  $\frac{1}{2}$ . The rule of pairwise occurrence is not valid for the horizontal *fourfold* axes in cubic space groups; here, *all* heights are given, including  $h = 0$  and  $\frac{1}{2}$ . This applies also to the horizontal  $\bar{4}$  axes and the  $\bar{4}$  inversion points located on these axes.



# International Tables for Crystallography

System	Axial lengths and angles	Bravais lattice	Lattice symbol
Cubic	Three equal axes at right angles $a = b = c$ , $\alpha = \beta = \gamma = 90^\circ$	Simple Body-centered Face-centered	P I F
Tetragonal	Three axes at right angles, two equal $a = b \neq c$ , $\alpha = \beta = \gamma = 90^\circ$	Simple Body-centered	P I
Orthorhombic	Three unequal axes at right angles $a \neq b \neq c$ , $\alpha = \beta = \gamma = 90^\circ$	Simple Body-centered Base-centered Face-centered	P I C F
Rhombohedral*	Three equal axes, equally inclined $a = b = c$ , $\alpha = \beta = \gamma \neq 90^\circ$	Simple	R
Hexagonal	Two equal coplanar axes at $120^\circ$ , third axis at right angles $a = b \neq c$ , $\alpha = \beta = 90^\circ$ , $\gamma = 120^\circ$	Simple	P
Monoclinic	Three unequal axes, one pair not at right angles $a \neq b \neq c$ , $\alpha = \gamma = 90^\circ \neq \beta$	Simple Base-centered	P C
Triclinic	Three unequal axes, unequally inclined and none at right angles $a \neq b \neq c$ , $\alpha \neq \beta \neq \gamma \neq 90^\circ$	Simple	P

\* Also called trigonal.



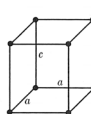
SIMPLE  
CUBIC (P)



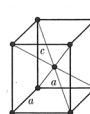
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CUBIC (I)



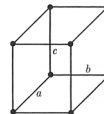
FACE-CENTERED  
CUBIC (F)



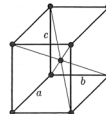
SIMPLE  
TETRAGONAL  
(P)



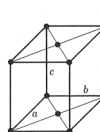
BODY-CENTERED  
TETRAGONAL  
(I)



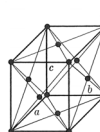
SIMPLE  
ORTHORHOMBIC  
(P)



BODY-CENTERED  
ORTHORHOMBIC  
(I)



BASE-CENTERED  
ORTHORHOMBIC  
(C)



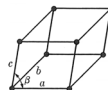
FACE-CENTERED  
ORTHORHOMBIC  
(F)



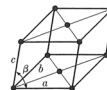
RHOMBOHEDRAL  
(R)



HEXAGONAL  
(P)



SIMPLE  
MONOCLINIC (P)



BASE-CENTERED  
MONOCLINIC (C)



TRICLINIC (P)

# International Tables for Crystallography

① CONTINUED

No. 35

$Cmm2$

② **Generators selected** (1);  $t(1,0,0)$ ;  $t(0,1,0)$ ;  $t(0,0,1)$ ;  $t(\frac{1}{2},\frac{1}{2},0)$ ; (2); (3)

③ **Positions**

Multiplicity,  
Wyckoff letter,  
Site symmetry

Coordinates

$(0,0,0)+(\frac{1}{2},\frac{1}{2},0)+$

Reflection conditions

General:

8  $f$  1 (1)  $x,y,z$  (2)  $\bar{x},\bar{y},z$  (3)  $x,\bar{y},z$  (4)  $\bar{x},y,z$

$hkl : h+k=2n$

$0kl : k=2n$

$h0l : h=2n$

$hkl : h+k=2n$

$h00 : h=2n$

$0k0 : k=2n$

Special: as above, plus

4  $e$   $m..$  0,y,z 0, $\bar{y}$ ,z

no extra conditions

4  $d$   $.m.$   $x,0,z$   $\bar{x},0,z$

no extra conditions

4  $c$   $..2$   $\frac{1}{2},\frac{1}{2},z$   $\frac{1}{2},\frac{1}{2},z$

$hkl : h=2n$

2  $b$   $m m 2$  0, $\frac{1}{2}$ ,z

no extra conditions

2  $a$   $m m 2$  0,0,z

no extra conditions

④ **Symmetry of special projections**

Along  $[001]$   $c2mm$

$a'=a$   $b'=b$

Origin at 0,0,z

Along  $[100]$   $p1m1$

$a'=\frac{1}{2}b$   $b'=c$

Origin at  $x,0,0$

Along  $[010]$   $p11m$

$a'=c$   $b'=\frac{1}{2}a$

Origin at 0,y,0

⑤ **Maximal non-isomorphic subgroups**

I [2] $C1m1$  ( $Cm$ , 8) (1; 3)+

[2] $Cm11$  ( $Cm$ , 8) (1; 4)+

[2] $C112$  ( $P2$ , 3) (1; 2)+

IIa [2] $Pba2$  (32) 1; 2; (3; 4) +  $(\frac{1}{2},\frac{1}{2},0)$

[2] $Pbm2$  ( $Pma2$ , 28) 1; 3; (2; 4) +  $(\frac{1}{2},\frac{1}{2},0)$

[2] $Pma2$  (28) 1; 4; (2; 3) +  $(\frac{1}{2},\frac{1}{2},0)$

[2] $Pmm2$  (25) 1; 2; 3; 4

IIb [2] $Ima2$  ( $c'=2c$ ) (46); [2] $Ibm2$  ( $c'=2c$ ) ( $Ima2$ , 46); [2] $Iba2$  ( $c'=2c$ ) (45); [2] $Imm2$  ( $c'=2c$ ) (44); [2] $Ccc2$  ( $c'=2c$ ) (37);

[2] $Cmc2_1$  ( $c'=2c$ ) (36); [2] $Ccm2_1$  ( $c'=2c$ ) ( $Cmc2_1$ , 36)

⑥ **Maximal isomorphic subgroups of lowest index**

IIc [2] $Cmm2$  ( $c'=2c$ ) (35); [3] $Cmm2$  ( $a'=3a$  or  $b'=3b$ ) (35)

⑦ **Minimal non-isomorphic supergroups**

I [2] $Cmmm$  (65); [2] $Cmme$  (67); [2] $P4mm$  (99); [2] $P4bm$  (100); [2] $P4_2cm$  (101); [2] $P4_2nm$  (102); [2] $P\bar{4}2m$  (111);

[2] $P\bar{4}2_1m$  (113); [3] $P6mm$  (183)

II [2] $Fmm2$  (42); [2] $Pmm2$  ( $a'=\frac{1}{2}a$ ,  $b'=\frac{1}{2}b$ ) (25)

# International Tables for Crystallography

① *Headline in abbreviated form.*

② *Generators selected:* Sections 2.2.10 and 8.3.5. A set of generators, as selected for these *Tables*, is listed in the form of translations and numbers of general-position coordinates. The generators determine the sequence of the coordinate triplets in the general position and of the corresponding symmetry operations.

③ *Positions:* Sections 2.2.11 and 8.3.2. The general Wyckoff position is given at the top, followed downwards by the various special Wyckoff positions with decreasing multiplicity and increasing site symmetry. For each general and special position its multiplicity, Wyckoff letter, oriented site-symmetry symbol, as well as the appropriate coordinate triplets and the reflection conditions, are listed. The coordinate triplets of the general position are numbered sequentially; cf. *Symmetry operations*.

*Oriented site-symmetry symbol* (third column): Section 2.2.12. The site symmetry at the points of a special position is given in oriented form.

*Reflection conditions* (right-most column): Section 2.2.13.

[*Lattice complexes* are described in Part 14; Tables 14.2.3.1 and 14.2.3.2 show the assignment of Wyckoff positions to Wyckoff sets and to lattice complexes.]

④ *Symmetry of special projections:* Section 2.2.14. For each space group, orthographic projections along three (symmetry) directions are listed. Given are the projection direction, the plane group of the projection, as well as the axes and the origin of the projected cell.

⑤ *Maximal non-isomorphic subgroups:* Sections 2.2.15 and 8.3.3.

Type **I**: *translationengleiche* or *t* subgroups;

Type **IIa**: *klassengleiche* or *k* subgroups, obtained by 'decentring' the conventional cell; applies only to space groups with centred cells;

Type **IIb**: *klassengleiche* or *k* subgroups, obtained by enlarging the conventional cell.

Given are:

For types **I** and **IIa**: Index [between brackets]; 'unconventional' Hermann–Mauguin symbol of the subgroup; 'conventional' Hermann–Mauguin symbol of the subgroup, if different (between parentheses); coordinate triplets retained in subgroup.

For type **IIb**: Index [between brackets]; 'unconventional' Hermann–Mauguin symbol of the subgroup; basis–vector relations between group and subgroup (between parentheses); 'conventional' Hermann–Mauguin symbol of the subgroup, if different (between parentheses).

⑥ *Maximal isomorphic subgroups of lowest index:* Sections 2.2.15, 8.3.3 and 13.1.2.

Type **IIc**: *klassengleiche* or *k* subgroups of lowest index which are of the same type as the group, i.e. have the same standard Hermann–Mauguin symbol. Data as for subgroups of type **IIb**.

⑦ *Minimal non-isomorphic supergroups:* Sections 2.2.15 and 8.3.3.

The list contains the reverse relations of the subgroup tables; only types **I** (*t* supergroups) and **II** (*k* supergroups) are distinguished. Data as for subgroups of type **IIb**.

# Problems describing a structure – Rhombohedral unit cell

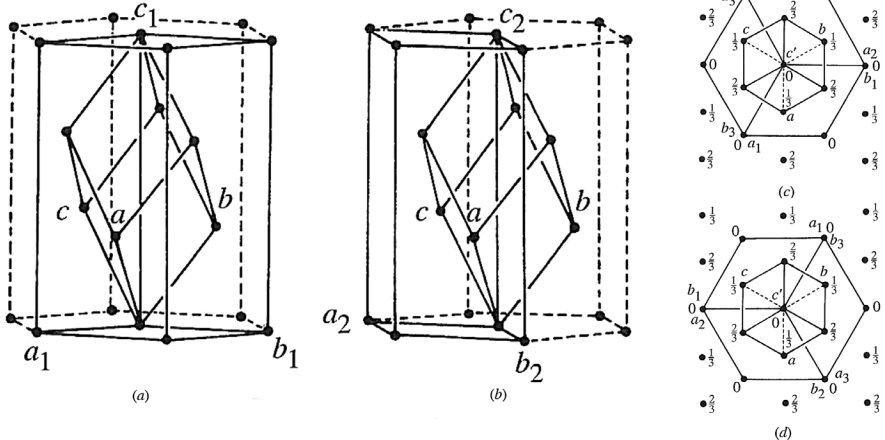


Fig. 5.1.3.6. Unit cells in the rhombohedral lattice: same origin for all cells. The basis of the rhombohedral cell is labelled  $a, b, c$ . Two settings of the triple hexagonal cell are possible with respect to a primitive rhombohedral cell: The *obverse setting* with the lattice points  $0, 0, 0; \frac{1}{3}, \frac{1}{3}, \frac{2}{3}; \frac{2}{3}, \frac{2}{3}, \frac{1}{3}$  has been used in *International Tables* since 1952. Its general reflection condition is  $-h + k + l = 3n$ . The *reverse setting* with lattice points  $0, 0, 0; \frac{1}{3}, \frac{2}{3}, \frac{1}{3}; \frac{2}{3}, \frac{1}{3}, \frac{2}{3}$  was used in the 1935 edition. Its general reflection condition is  $h - k + l = 3n$ . (a) Obverse setting of triple hexagonal cell  $a_1, b_1, c_1$  in relation to the primitive rhombohedral cell  $a, b, c$ . (b) Reverse setting of triple hexagonal cell  $a_2, b_2, c_2$  in relation to the primitive rhombohedral cell  $a, b, c$ . (c) Primitive rhombohedral cell (--- lower edges),  $a, b, c$  in relation to the three triple hexagonal cells in obverse setting  $a_1, b_1, c'_1; a_2, b_2, c'_1; a_3, b_3, c'_1$ . Projection along  $c'$ . (d) Primitive rhombohedral cell (--- lower edges),  $a, b, c$  in relation to the three triple hexagonal cells in reverse setting  $a_1, b_1, c'_1; a_2, b_2, c'_1; a_3, b_3, c'_1$ . Projection along  $c'$ .

# Problems describing a structure – Rhombohedral unit cell

**R3**

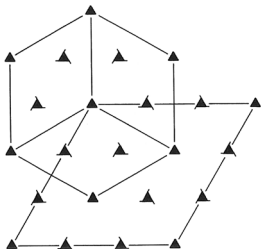
**$C_3^4$**

3

No. 146

**R3**

HEXAGONAL AXES



**Generators selected** (1);  $r(1,0,0)$ ;  $r(0,1,0)$ ;  $r(0,0,1)$ ;  $r(\frac{1}{3}, \frac{1}{3}, \frac{1}{3})$ ; (2)

## Positions

Multiplicity, Wyckoff letter, Site symmetry	Coordinates		
	$(0,0,0)+$	$(\frac{1}{3}, \frac{1}{3}, \frac{1}{3})+$	$(\frac{2}{3}, \frac{2}{3}, \frac{2}{3})+$

9	$b$	1	(1) $x, y, z$	(2) $\bar{y}, x - y, z$	(3) $\bar{x} + y, \bar{x}, z$
---	-----	---	---------------	-------------------------	-------------------------------

3	$a$	3.	0,0,z
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## Symmetry of special projections

Along  $[001]$   $p3$   
 $\mathbf{a}' = \frac{1}{3}(2\mathbf{a} + \mathbf{b})$   
 Origin at 0,0,z

$\mathbf{b}' = \frac{1}{3}(-\mathbf{a} + \mathbf{b})$

Along  $[100]$   $p1$   
 $\mathbf{a}' = \frac{1}{3}(\mathbf{a} + 2\mathbf{b})$   
 Origin at  $x,0,0$

$\mathbf{b}' = \frac{1}{3}(-\mathbf{a} - 2\mathbf{b} + \mathbf{c})$

**R3**

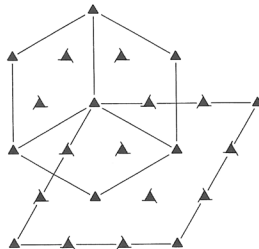
**$C_3^4$**

3

No. 146

**R3**

RHOMBOHEDRAL AXES



**Generators selected** (1);  $r(1,0,0)$ ;  $r(0,1,0)$ ;  $r(0,0,1)$ ; (2)

## Positions

Multiplicity, Wyckoff letter, Site symmetry	Coordinates		
	$(1) x, y, z$	$(2) z, x, y$	$(3) y, z, x$

3	$b$	1	(1) $x, y, z$	(2) $z, x, y$	(3) $y, z, x$
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1	$a$	3.	$x, x, x$
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## Symmetry of special projections

Along  $[111]$   $p3$   
 $\mathbf{a}' = \frac{1}{3}(2\mathbf{a} - \mathbf{b} - \mathbf{c})$   
 Origin at  $x, x, x$

$\mathbf{b}' = \frac{1}{3}(-\mathbf{a} + 2\mathbf{b} - \mathbf{c})$

Along  $[1\bar{1}0]$   $p1$   
 $\mathbf{a}' = \frac{1}{3}(\mathbf{a} + \mathbf{b} - 2\mathbf{c})$   
 Origin at  $x, \bar{x}, 0$

$\mathbf{b}' = \mathbf{c}$

# Problems describing a structure – Origin of cell

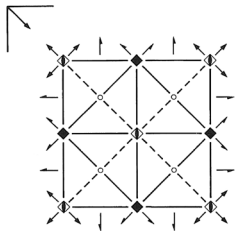
$P4/nmm$

$D_{4h}^7$

No. 129

$P 4/n 2_1/m 2/m$

ORIGIN CHOICE 1



**Origin** at  $\bar{4}m2$  at  $\bar{4}/nm2/g$ , at  $-\frac{1}{2}, \frac{1}{2}, 0$  from centre  $(2/m)$

**Asymmetric unit**  $0 \leq x \leq \frac{1}{2}; 0 \leq y \leq \frac{1}{2}; 0 \leq z \leq \frac{1}{2}; y \leq \frac{1}{2} - x$

**Symmetry operations**

- |  |   |  |
|--|---|--|
| (1) 1  | (2) $2 \quad 0,0,z$                                 | (3) $4^+ \quad 0, \frac{1}{2}, z$          |
| (5) $2(0, \frac{1}{2}, 0) \quad \frac{1}{2}, y, 0$ | (6) $2(\frac{1}{2}, 0, 0) \quad x, \frac{1}{2}, 0$  | (7) $2 \quad x, x, 0$                      |
| (9) $\bar{1} \quad \frac{1}{2}, \frac{1}{2}, 0$    | (10) $n(\frac{1}{2}, \frac{1}{2}, 0) \quad x, y, 0$ | (11) $\bar{4}^+ \quad 0, 0, z; 0, 0, 0$    |
| (13) $m \quad x, 0, z$                             | (14) $m \quad 0, y, z$                              | (15) $m \quad x + \frac{1}{2}, \bar{x}, z$ |

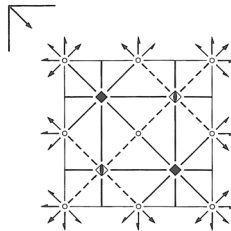
$P4/nmm$

$D_{4h}^7$

No. 129

$P 4/n 2_1/m 2/m$

ORIGIN CHOICE 2



**Origin** at centre  $(2/m)$  at  $n2_1(2/m, 2_1/g)$ , at  $\frac{1}{2}, -\frac{1}{2}, 0$  from  $\bar{4}m2$

**Asymmetric unit**  $-\frac{1}{2} \leq x \leq \frac{1}{2}; -\frac{1}{2} \leq y \leq \frac{1}{2}; 0 \leq z \leq \frac{1}{2}; x \leq y$

**Symmetry operations**

- |  |   |   |
|--|---|---|
| (1) 1                                    | (2) $2 \quad \frac{1}{2}, \frac{1}{2}, z$           | (3) $4^+ \quad \frac{1}{2}, \frac{1}{2}, z$                                       |
| (5) $2(0, \frac{1}{2}, 0) \quad 0, y, 0$ | (6) $2(\frac{1}{2}, 0, 0) \quad x, 0, 0$            | (7) $2(\frac{1}{2}, \frac{1}{2}, 0) \quad x, x, 0$                                |
| (9) $\bar{1} \quad 0, 0, 0$              | (10) $n(\frac{1}{2}, \frac{1}{2}, 0) \quad x, y, 0$ | (11) $\bar{4}^+ \quad \frac{1}{2}, -\frac{1}{2}, z; \frac{1}{2}, -\frac{1}{2}, 0$ |
| (13) $m \quad x, \frac{1}{2}, z$         | (14) $m \quad \frac{1}{2}, y, z$                    | (15) $m \quad x + \frac{1}{2}, \bar{x}, z$  |

# Problems describing a structure – Origin of cell

$P4/nmm$

$D_{4h}^7$

No. 129

$P 4/n 2_1/m 2/m$

ORIGIN CHOICE 1

## Positions

Multiplicity,  
Wyckoff letter,  
Site symmetry

Coordinates

16	$k$	1	(1) $x, y, z$ (5) $\bar{x} + \frac{1}{2}, y + \frac{1}{2}, \bar{z}$ (9) $\bar{x} + \frac{1}{2}, \bar{y} + \frac{1}{2}, \bar{z}$ (13) $x, \bar{y}, z$	(2) $\bar{x}, \bar{y}, z$ (6) $x + \frac{1}{2}, \bar{y} + \frac{1}{2}, \bar{z}$ (10) $x + \frac{1}{2}, y + \frac{1}{2}, \bar{z}$ (14) $\bar{x}, y, z$	(3) $\bar{y} + \frac{1}{2}, x + \frac{1}{2}, z$ (7) $y, x, \bar{z}$ (11) $y, \bar{x}, \bar{z}$ (15) $\bar{y} + \frac{1}{2}, \bar{x} + \frac{1}{2}, z$
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8	$j$	$\dots m$	$x, x + \frac{1}{2}, z$ $\bar{x} + \frac{1}{2}, x, \bar{z}$	$\bar{x}, \bar{x} + \frac{1}{2}, z$ $x + \frac{1}{2}, \bar{x}, \bar{z}$	$\bar{x}, x + \frac{1}{2}, z$ $x + \frac{1}{2}, x, \bar{z}$	$x, \bar{x} + \frac{1}{2}, z$ $\bar{x} + \frac{1}{2}, \bar{x}, \bar{z}$
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8	$i$	$\dots m$	$0, y, z$ $\frac{1}{2}, y + \frac{1}{2}, \bar{z}$	$0, \bar{y}, z$ $\frac{1}{2}, \bar{y} + \frac{1}{2}, \bar{z}$	$\bar{y} + \frac{1}{2}, \frac{1}{2}, z$ $y, 0, \bar{z}$	$y + \frac{1}{2}, \frac{1}{2}, z$ $\bar{y}, 0, \bar{z}$
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8	$h$	$\dots 2$	$x, x, \frac{1}{2}$ $\bar{x} + \frac{1}{2}, \bar{x} + \frac{1}{2}, \frac{1}{2}$	$\bar{x}, \bar{x}, \frac{1}{2}$ $x + \frac{1}{2}, x + \frac{1}{2}, \frac{1}{2}$	$\bar{x} + \frac{1}{2}, x + \frac{1}{2}, \frac{1}{2}$ $x, \bar{x}, \frac{1}{2}$	$x, \bar{x} + \frac{1}{2}, \frac{1}{2}$ $\bar{x} + \frac{1}{2}, \bar{x}, \frac{1}{2}$
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8	$g$	$\dots 2$	$x, x, 0$ $\bar{x} + \frac{1}{2}, \bar{x} + \frac{1}{2}, 0$	$\bar{x}, \bar{x}, 0$ $x + \frac{1}{2}, x + \frac{1}{2}, 0$	$\bar{x} + \frac{1}{2}, x + \frac{1}{2}, 0$ $x, \bar{x}, 0$	$x, \bar{x} + \frac{1}{2}, 0$ $\bar{x} + \frac{1}{2}, \bar{x}, 0$
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4	$f$	$2mm$	$0, 0, z$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$0, 0, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$0, 0, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$
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4	$e$	$\dots 2/m$	$\frac{1}{4}, \frac{1}{4}, \frac{1}{2}$ $\frac{3}{4}, \frac{3}{4}, \frac{1}{2}$	$\frac{3}{4}, \frac{1}{4}, \frac{1}{2}$ $\frac{1}{4}, \frac{3}{4}, \frac{1}{2}$	$\frac{1}{4}, \frac{1}{4}, \frac{1}{2}$ $\frac{3}{4}, \frac{3}{4}, \frac{1}{2}$	$\frac{3}{4}, \frac{1}{4}, \frac{1}{2}$ $\frac{1}{4}, \frac{3}{4}, \frac{1}{2}$
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4	$d$	$\dots 2/m$	$\frac{1}{2}, \frac{1}{4}, 0$ $\frac{3}{2}, \frac{3}{4}, 0$	$\frac{1}{2}, \frac{3}{4}, 0$ $\frac{1}{2}, \frac{1}{4}, 0$	$\frac{1}{2}, \frac{1}{4}, 0$ $\frac{3}{2}, \frac{3}{4}, 0$	$\frac{1}{2}, \frac{3}{4}, 0$ $\frac{1}{2}, \frac{1}{4}, 0$
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2	$c$	$4mm$	$0, \frac{1}{2}, z$ $\frac{1}{2}, 0, \bar{z}$	$\frac{1}{2}, 0, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, z$	$\frac{1}{2}, 0, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, z$	$\frac{1}{2}, 0, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, z$
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2	$b$	$\bar{4}m2$	$0, 0, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$
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2	$a$	$\bar{4}m2$	$0, 0, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$
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$P4/nmm$

$D_{4h}^7$

No. 129

$P 4/n 2_1/m 2/m$

ORIGIN CHOICE 2

## Positions

Multiplicity,  
Wyckoff letter,  
Site symmetry

Coordinates

16	$k$	1	(1) $x, y, z$ (5) $\bar{x}, y + \frac{1}{2}, \bar{z}$ (9) $\bar{x}, \bar{y}, \bar{z}$ (13) $x, \bar{y} + \frac{1}{2}, z$	(2) $\bar{x} + \frac{1}{2}, \bar{y} + \frac{1}{2}, z$ (6) $x + \frac{1}{2}, \bar{y}, \bar{z}$ (10) $x + \frac{1}{2}, y + \frac{1}{2}, \bar{z}$ (14) $\bar{x} + \frac{1}{2}, y, z$	(3) $\bar{y} + \frac{1}{2}, x, z$ (7) $y + \frac{1}{2}, x + \frac{1}{2}, \bar{z}$ (11) $y + \frac{1}{2}, \bar{x}, \bar{z}$ (15) $\bar{y} + \frac{1}{2}, \bar{x} + \frac{1}{2}, z$
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8	$j$	$\dots m$	$x, x, z$ $\bar{x}, x + \frac{1}{2}, \bar{z}$	$\bar{x} + \frac{1}{2}, \bar{x} + \frac{1}{2}, z$ $x + \frac{1}{2}, \bar{x}, \bar{z}$	$\bar{x} + \frac{1}{2}, x, z$ $x + \frac{1}{2}, x + \frac{1}{2}, \bar{z}$	$x, \bar{x} + \frac{1}{2}, z$ $\bar{x}, \bar{x}, \bar{z}$
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8	$i$	$\dots m$	$\frac{1}{2}, y, z$ $\frac{1}{2}, y + \frac{1}{2}, \bar{z}$	$\frac{1}{2}, \bar{y} + \frac{1}{2}, z$ $\frac{1}{2}, \bar{y}, \bar{z}$	$\bar{y} + \frac{1}{2}, \frac{1}{2}, z$ $y + \frac{1}{2}, \frac{1}{2}, \bar{z}$	$y, \frac{1}{2}, z$ $\bar{y}, \frac{1}{2}, \bar{z}$
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8	$h$	$\dots 2$	$x, \bar{x}, \frac{1}{2}$ $\bar{x}, x, \frac{1}{2}$	$\bar{x} + \frac{1}{2}, x + \frac{1}{2}, \frac{1}{2}$ $x + \frac{1}{2}, \bar{x} + \frac{1}{2}, \frac{1}{2}$	$x + \frac{1}{2}, x, \frac{1}{2}$ $\bar{x} + \frac{1}{2}, \bar{x}, \frac{1}{2}$	$\bar{x}, \bar{x} + \frac{1}{2}, \frac{1}{2}$ $x, x + \frac{1}{2}, \frac{1}{2}$
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8	$g$	$\dots 2$	$x, \bar{x}, 0$ $\bar{x}, x, 0$	$\bar{x} + \frac{1}{2}, x + \frac{1}{2}, 0$ $x + \frac{1}{2}, \bar{x} + \frac{1}{2}, 0$	$x + \frac{1}{2}, x, 0$ $\bar{x} + \frac{1}{2}, \bar{x}, 0$	$\bar{x}, \bar{x} + \frac{1}{2}, 0$ $x, x + \frac{1}{2}, 0$
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4	$f$	$2mm$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, z$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, z$	$\frac{1}{2}, \frac{1}{2}, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$	$\frac{1}{2}, \frac{1}{2}, \bar{z}$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$
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4	$e$	$\dots 2/m$	$0, 0, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, 0, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$0, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$
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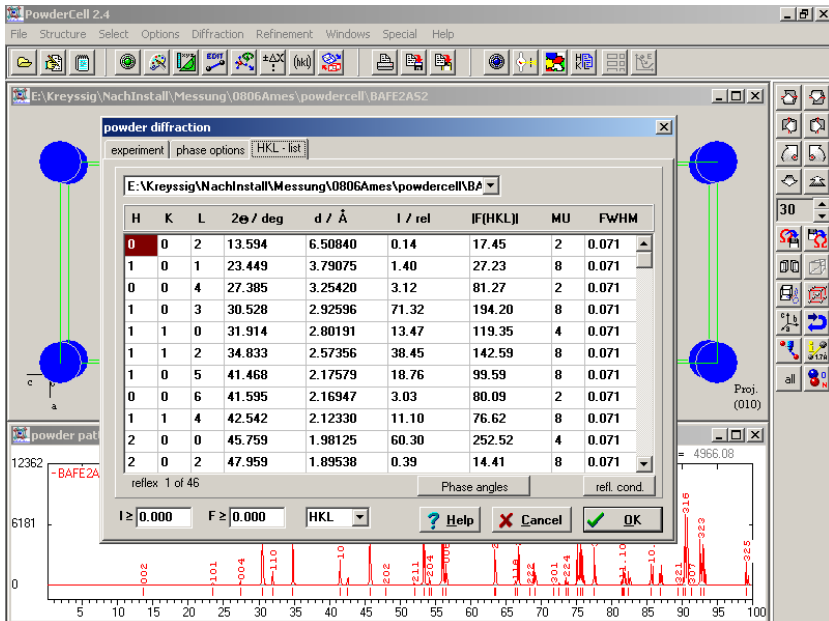
4	$d$	$\dots 2/m$	$0, 0, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, 0, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$0, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$
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2	$c$	$4mm$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$	$\frac{1}{2}, \frac{1}{2}, z$ $\frac{1}{2}, \frac{1}{2}, \bar{z}$
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2	$b$	$\bar{4}m2$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$	$\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$ $\frac{1}{2}, \frac{1}{2}, \frac{1}{2}$
---	-----	-------------	--	--	--	--

2	$a$	$\bar{4}m2$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$	$\frac{1}{2}, \frac{1}{2}, 0$ $\frac{1}{2}, \frac{1}{2}, 0$
---	-----	-------------	--	--	--	--

# Powdercell



Extract the reflection list: (hkl) – position - intensity



## Preparation of a reflection list for further use

1. Collect a diffraction pattern from the pure phase. If pure phase material is not available, then the phase should constitute the bulk of the sample.
2. Run the Rietveld program in the LeBail fitting mode using the assigned space group and unit cell parameters. From the refined list of intensities, create a file containing  $h$ ,  $k$ ,  $l$ ,  $M$ ,  $d$ ,  $2\theta$  and  $I$ , where  $h$ ,  $k$  and  $l$  are the Miller indices of the reflection,  $M$  is the reflection multiplicity,  $d$  is the  $d$ -spacing of the reflection,  $2\theta$  is the Bragg angle and  $I$  is the reflection intensity.
3. Depending on which Rietveld program has been used, it might be necessary to remove the effect of the Lorentz-polarization ( $Lp$ ) factor from each observed peak intensity:

$$Lp = \frac{1 + \cos^2 2\alpha \cdot \cos^2 2\theta}{4 \cos \theta \sin^2 \theta \cdot (1 + \cos^2 2\alpha)}$$

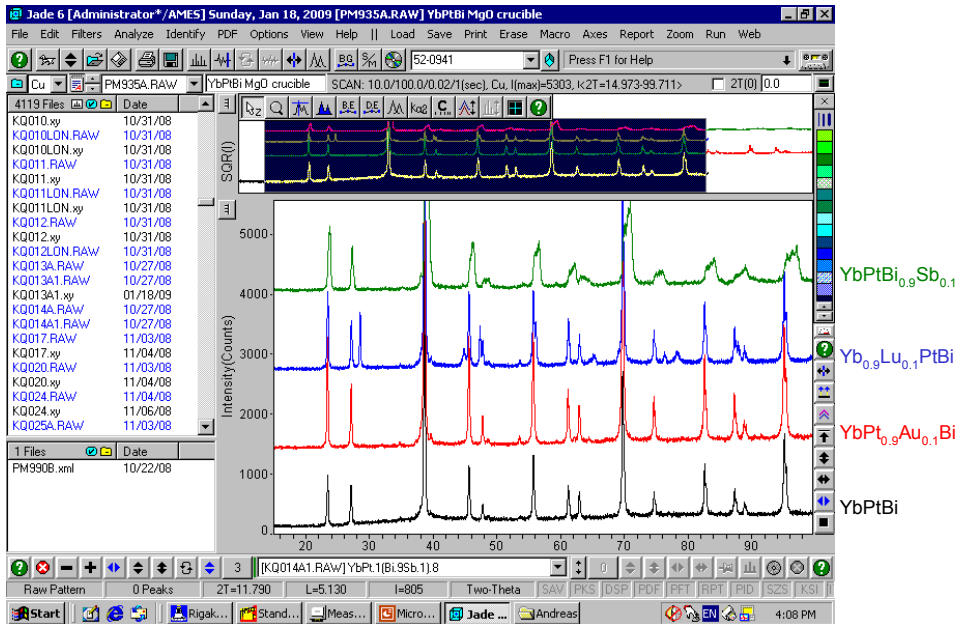
where  $\alpha$  is the diffraction angle of the monochromator.

Note that Equation (23) refers to Bragg–Brentano geometry.

4. Removal of the contribution of the  $Lp$  factor from the measured intensities *via*:

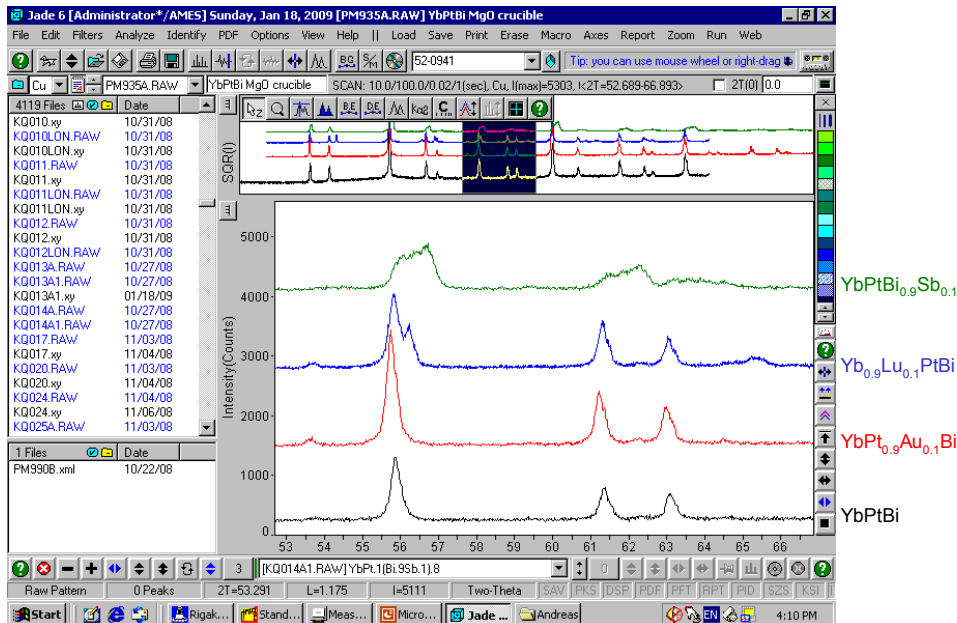
$$I'_{\text{meas}} = \frac{I_{\text{meas}}}{Lp}$$

# Example: growth of YbPtBi with partial element substitution



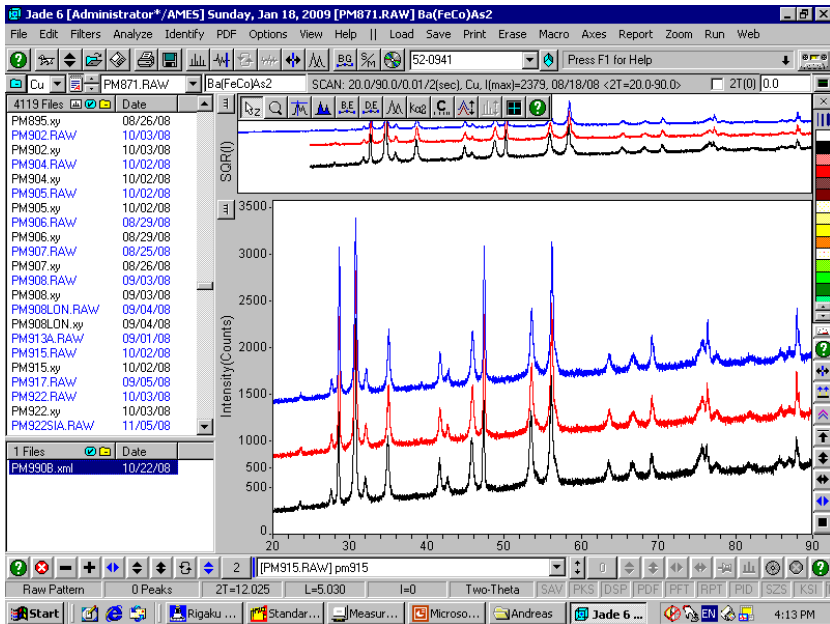
Which phases were grown successfully?

# Example: growth of YbPtBi with partial element substitution



Only YbPt<sub>0.9</sub>Au<sub>0.1</sub>Bi was grown successfully.

# Example: growth of $\text{Ba}(\text{Fe}_{1-x}\text{Co}_x)_2\text{As}_2$



$x = 0.10$

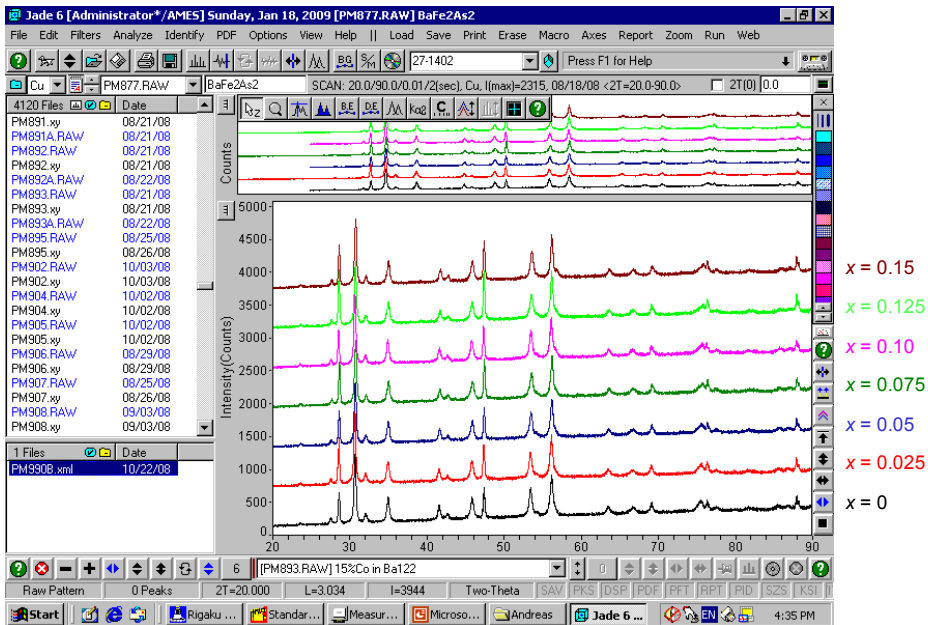
PM915

PM892

PM871

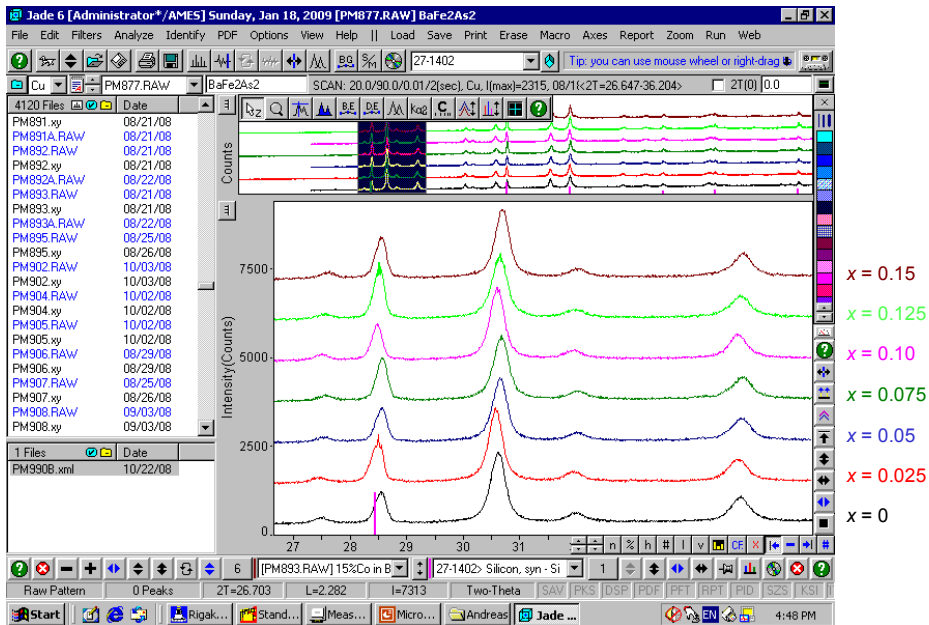
Preparation of samples with same stoichiometry is reproducible.

# Example: growth of $\text{Ba}(\text{Fe}_{1-x}\text{Co}_x)_2\text{As}_2$



Preparation of samples with varying stoichiometry seems also successful.

# Example: growth of $\text{Ba}(\text{Fe}_{1-x}\text{Co}_x)_2\text{As}_2$



Use of “inner” standard a MUST.

# Position of Bragg reflections in powder pattern

$$\lambda = 2d_{hkl} \sin \theta$$

$$\frac{1}{d^2} = \frac{1}{V^2} (S_{11}h^2 + S_{22}k^2 + S_{33}l^2 + 2S_{12}hk + 2S_{13}hl + 2S_{23}kl)$$

$$V = abc \sqrt{1 - \cos^2 \alpha - \cos^2 \beta - \cos^2 \gamma + 2 \cos \alpha \cos \beta \cos \gamma}$$

$$S_{11} = b^2 c^2 \sin^2 \alpha$$

$$S_{22} = a^2 c^2 \sin^2 \beta$$

$$S_{33} = a^2 b^2 \sin^2 \gamma$$

$$S_{12} = abc^2 (\cos \alpha \cos \beta - \cos \gamma)$$

$$S_{13} = ab^2 c (\cos \gamma \cos \alpha - \cos \beta)$$

$$S_{23} = a^2 bc (\cos \beta \cos \gamma - \cos \alpha)$$

Factors affecting peak positions:

$$\Delta 2\theta = \frac{p_1}{\tan 2\theta} + \frac{p_2}{\sin 2\theta} + \frac{p_3}{\tan \theta} + p_4 \sin 2\theta + p_5 \cos \theta + p_6$$

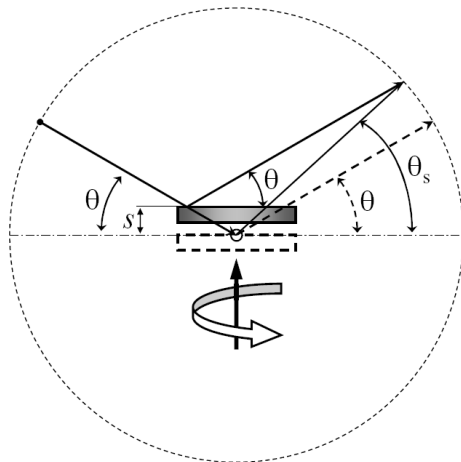
Asymmetry:  $p_1 = -\frac{h^2 K_1}{3R^2}; \quad p_2 = -\frac{h^2 K_2}{3R^2}$

In-plane divergence:  $p_3 = -\frac{\alpha^2}{K_3}$

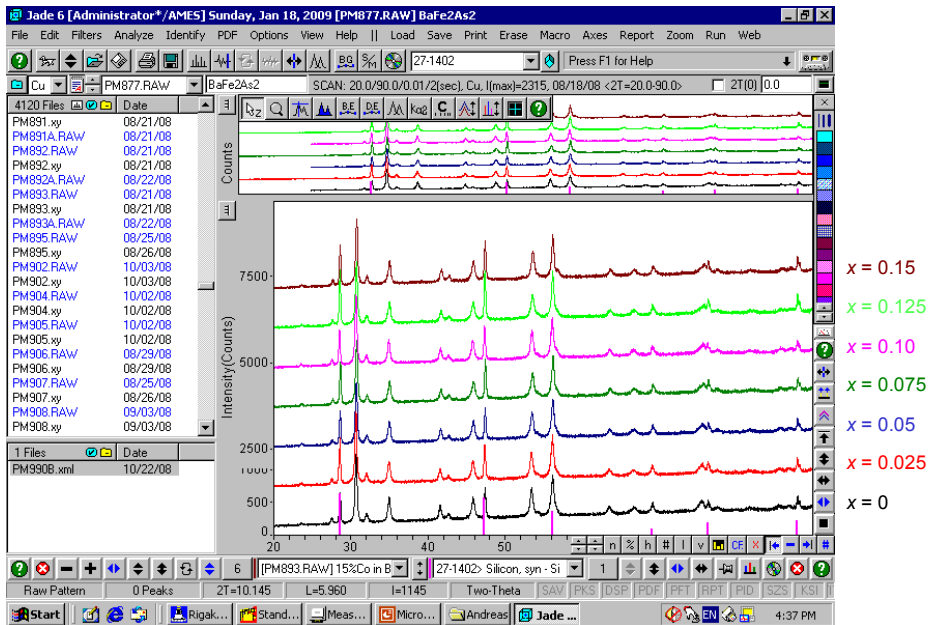
Transparency:  $p_4 = \frac{1}{2\mu_{\text{eff}} R}$

Sample displacement:  $p_5 = -\frac{2s}{R}$

Zero shift:  $p_6$



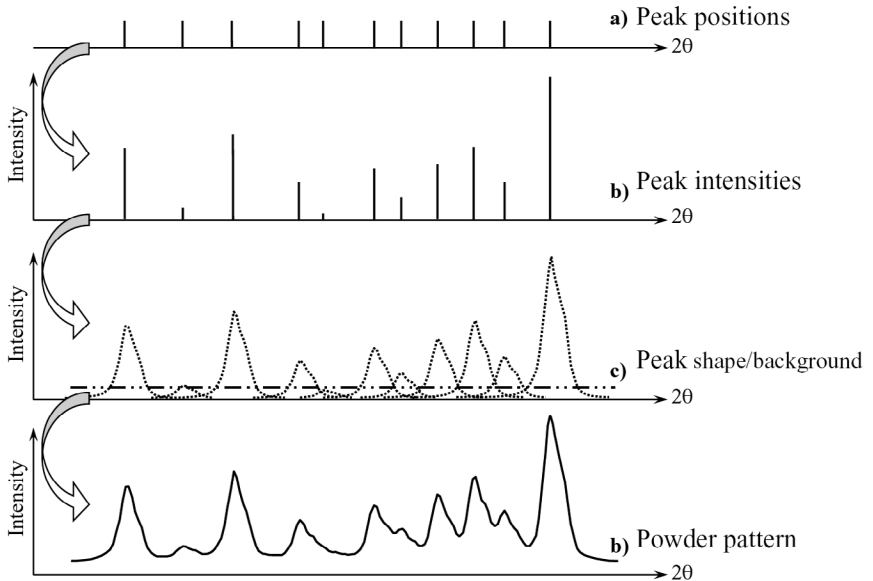
# Example: growth of $\text{Ba}(\text{Fe}_{1-x}\text{Co}_x)_2\text{As}_2$



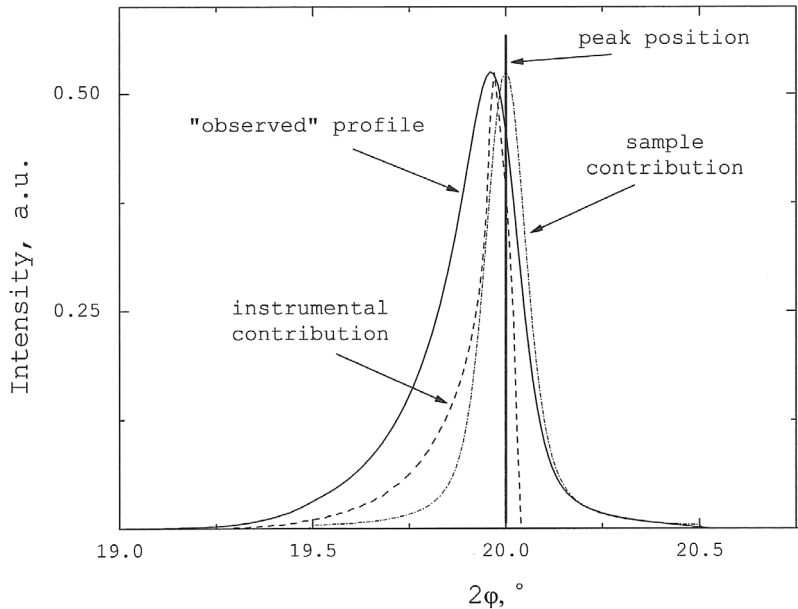
Combined analysis of series of Bragg reflections (main phase + standard) necessary.



# Combined fitting of Bragg reflections



# Profile of Bragg reflections in powder pattern



# Profile of Bragg reflections in powder pattern

Gaussian

$$G = I_0 \exp \left( -\ln 2 \left( \frac{2\Theta - 2\Theta_0}{\omega} \right)^2 \right)$$

Lorentzian

$$L = I_0 \left( 1 + \left( \frac{2\Theta - 2\Theta_0}{\omega} \right)^2 \right)^{-n} \quad n = 1, 1.5, 2$$

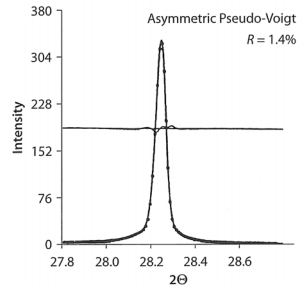
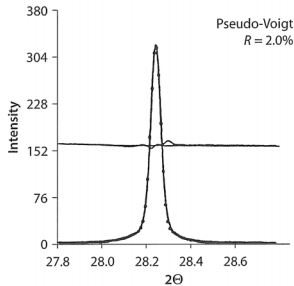
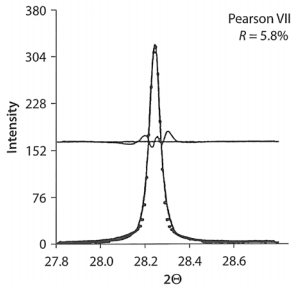
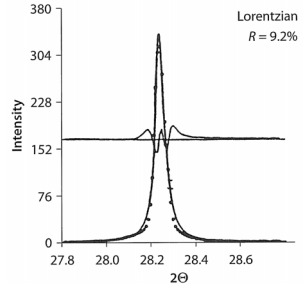
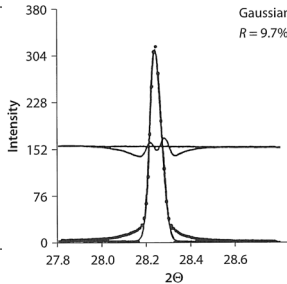
Pseudo-Voigt

$$V = \eta L + (1 - \eta)G \quad (0 \leq \eta \leq 1)$$

Pearson VII

$$P = I_0 \left( 1 + \left( \frac{2\Theta - 2\Theta_0}{m\sigma^2} \right)^2 \right)^{-m}$$

Parameter:  $2\Theta_0$  = peak position;  $I_0$  = peak intensity;  $\omega$  =  $FWHM/2$ ;  $m$  = shape parameter.



## **R-values (residuals) – reliability criteria for refinements**

$$R = \frac{\sum_i |y_i(\text{obs}) - y_i(\text{calc})|}{\sum_i |y_i(\text{obs})|}$$

$$R_{wp} = \frac{\sqrt{\sum_i w_i (y_i(\text{obs}) - y_i(\text{calc}))^2}}{\sqrt{\sum_i w_i y_i(\text{obs})^2}}$$

$$R_{\text{exp}} = \frac{\sqrt{n-m}}{\sqrt{\sum_i w_i y_i(\text{obs})^2}}$$

$$M = \left( \sum_i w_i (y_i(\text{obs}) - y_i(\text{calc}))^2 \right)^{1/2}$$

$$R_{\text{Bragg}} = \frac{\sum_j |I_j(\text{obs}) - I_j(\text{calc})|}{\sum_j |I_j(\text{obs})|}$$

## Example: growth of $\text{Ba}(\text{Fe}_{1-x}\text{Co}_x)_2\text{As}_2$

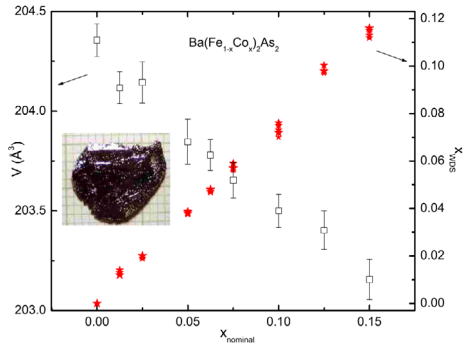


FIG. 2. (Color online) Unit-cell volume and Co concentration determined from WDS measurement as a function of nominal Co concentration. Multiple WDS data points were collected for each nominal  $x$  and are each plotted, giving a sense of measured variation in Co concentration. Inset: picture of a representative single crystal over a millimeter grid.

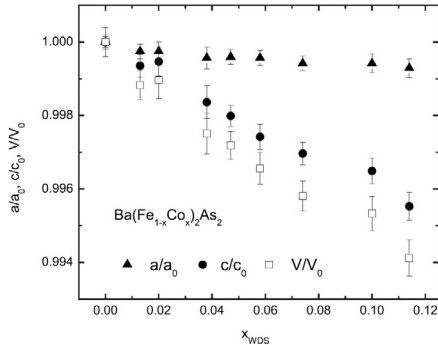
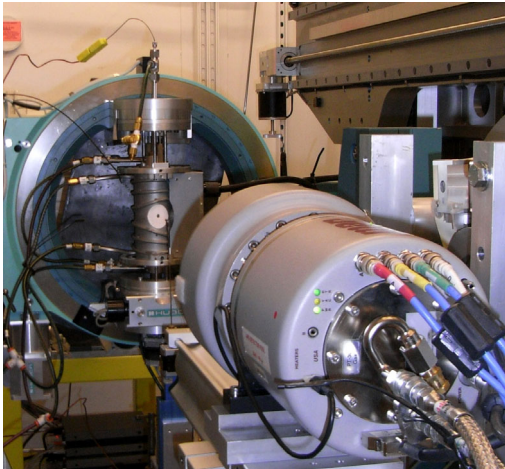


FIG. 3. Unit cell parameters,  $a$  and  $c$ , as well as unit-cell volume,  $V$ , normalized to  $a_0 = 3.9621 \text{ \AA}$ ,  $c_0 = 13.0178 \text{ \AA}$ , and  $V_0 = 204.3565 \text{ \AA}^3$  of undoped  $\text{BaFe}_2\text{As}_2$  as a function of measured concentration of Co,  $x_{\text{WDS}}$ .

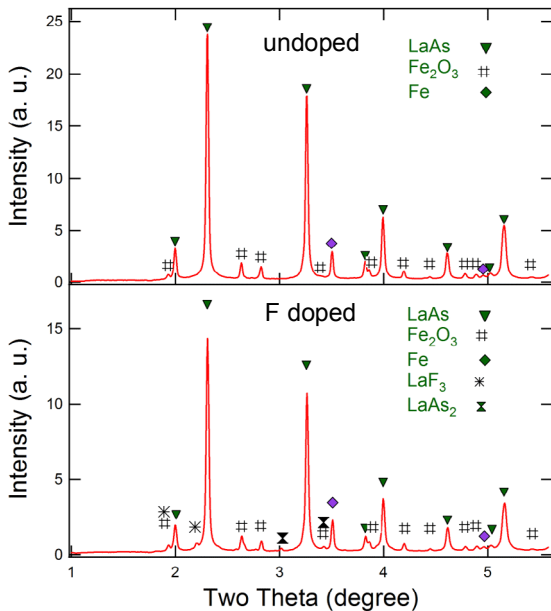
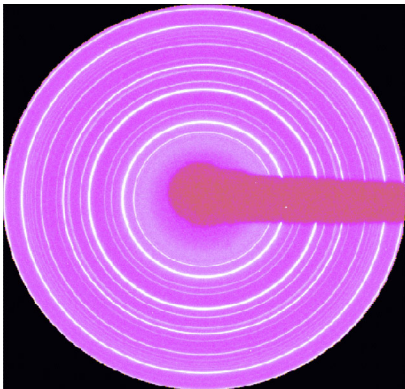
Realized stoichiometry by WDS study; Vegard's law for lattice parameter

## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$



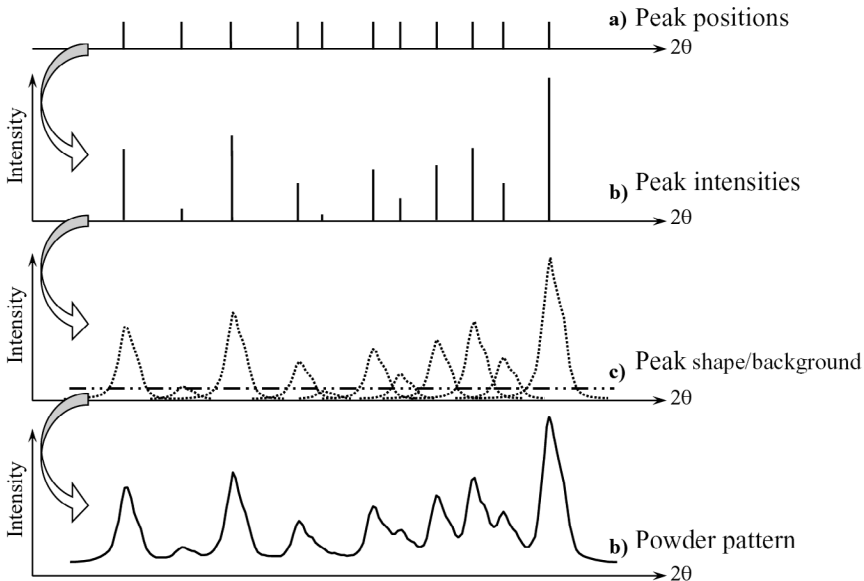
High-temperature x-ray diffraction with 2-dimensional detector

## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$



High-temperature x-ray diffraction with 2-dimensional detector

# Rietveld refinement of powder pattern





## Intensity of Bragg reflections in powder pattern

$$I_{hkl} = K \times p_{hkl} \times L_{\theta} \times P_{\theta} \times A_{\theta} \times T_{hkl} \times E_{hkl} \times |F_{hkl}|^2$$

Structure amplitude:

$$\mathbf{F}(\mathbf{h}) = \sum_{j=1}^n g^j t^j(s) f^j(s) \exp(2\pi i \mathbf{h} \cdot \mathbf{x}^j)$$

$K$  = scale factor

$p_{hkl}$  = multiplicity factor

$L_{\theta}$  = Lorentz factor

$P_{\theta}$  = polarization factor

$A_{\theta}$  = absorption factor

$T_{hkl}$  = preferred orientation factor

$E_{hkl}$  = extinction factor

$g^j$  = population

$t^j$  = Temperature factor

# Lorentz and Polarization factor

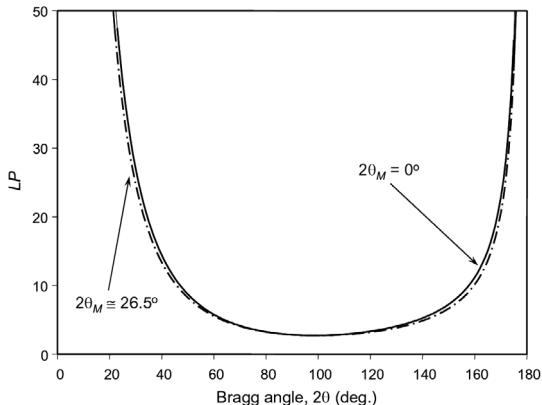
$L_\theta$  = Lorentz factor

$$L = \frac{1}{\cos \theta \sin^2 \theta}$$

$P_\theta$  = polarization factor

$$P \propto \frac{1 - K + K \cdot \cos^2 2\theta \cdot \cos^2 2\theta_M}{2}$$

$$LP = \frac{1 + \cos^2 2\theta \cos^2 2\theta_M}{\cos \theta \cdot \sin^2 \theta}, K=0.5$$



# Absorption factor

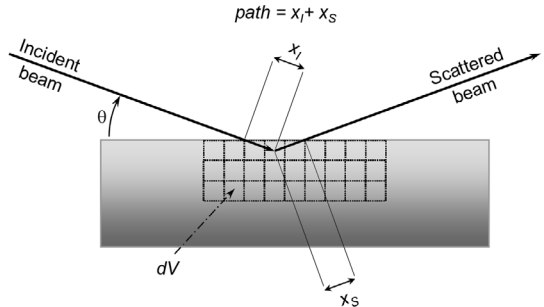
$A_\theta$  = absorption factor

$$A = \frac{1}{V} \int_V \exp(-\mu_{eff} l) dV$$

$$A = \frac{\mu_{eff}}{2} = \text{const (flat opaque sample)}$$

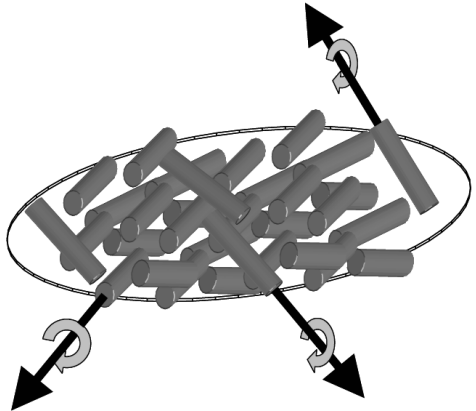
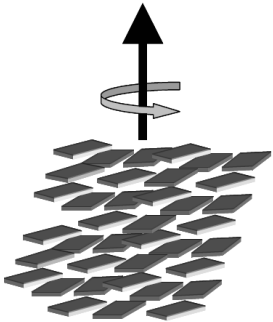
$$A = \frac{1 - \exp(-2\mu_{eff} t / \sin \theta)}{2\mu} \propto 1 - \exp(-2\mu_{eff} t / \sin \theta)$$

flat semitransparent sample



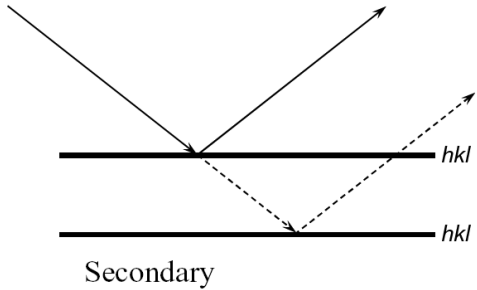
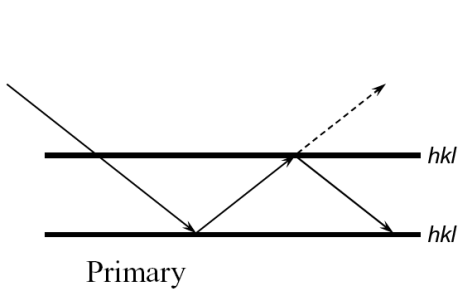
## Preferred orientation factor

$T_{hkl}$  = preferred orientation factor



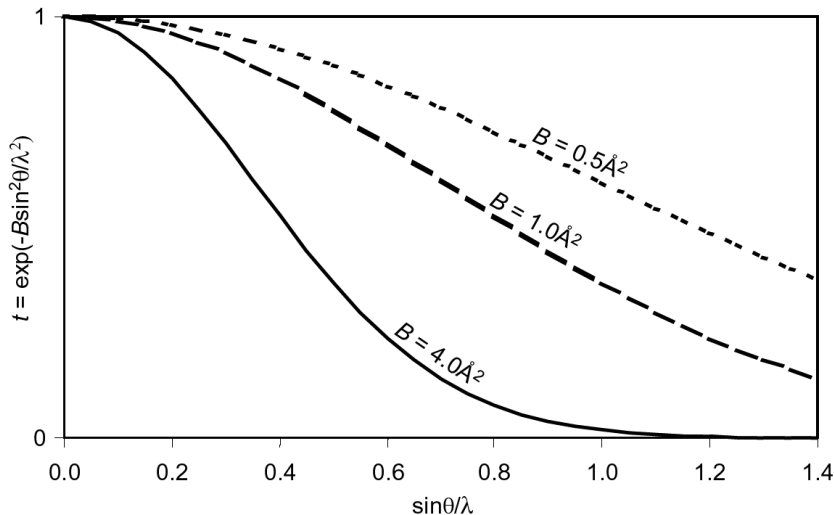
# Extinction factor

$E_{hkl}$  = extinction factor



## Temperature factor

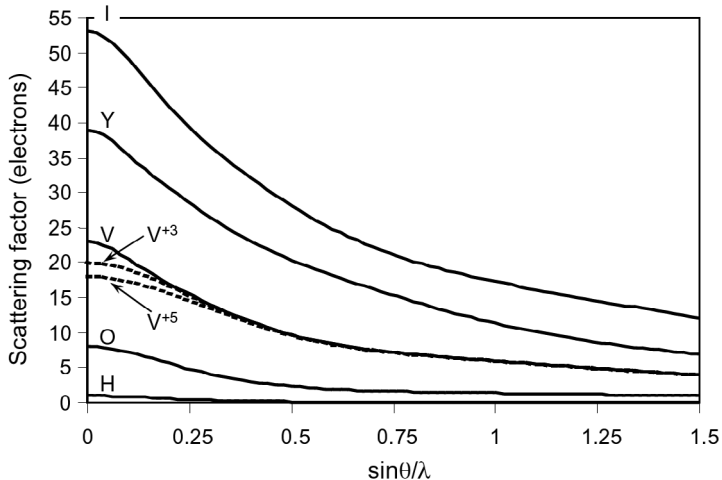
Temperature factor:  $t^j = \exp\left(-B^j \frac{\sin^2 \theta}{\lambda^2}\right)$  (isotropic)



# Atomic scattering factor

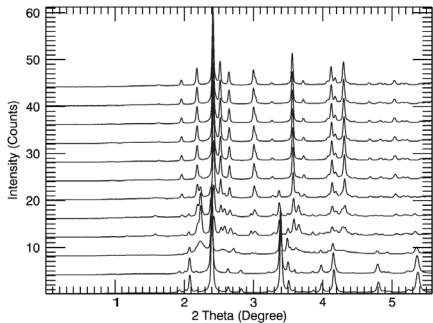
$f^j$  = atomic scattering factor (radial distribution of electrons for x-rays),  
constant for neutrons

Units:            Scattering ability of a single electron  
                    Coherent scattering length. Femtometer =  $10^{-15}$  m

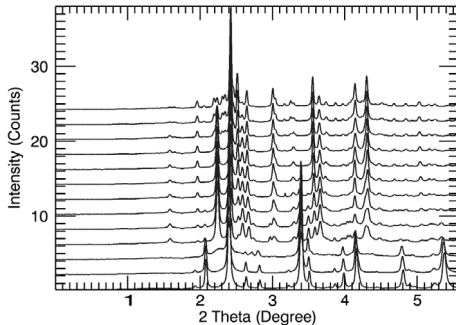


## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$

F doped



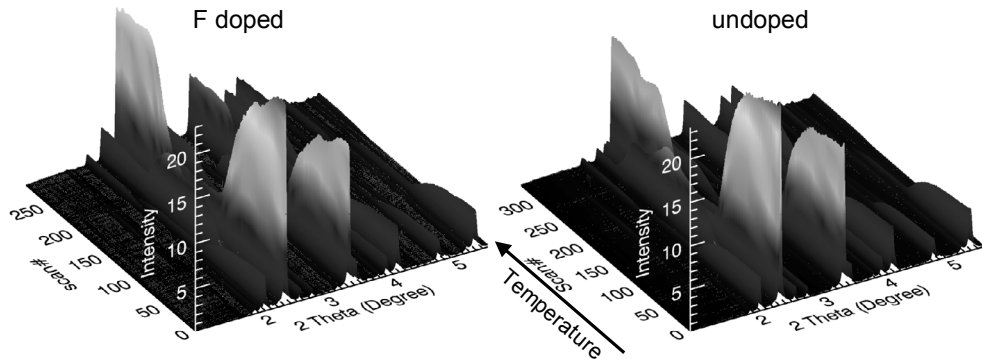
undoped



Temperature-dependent x-ray diffraction (20 sec. pattern)

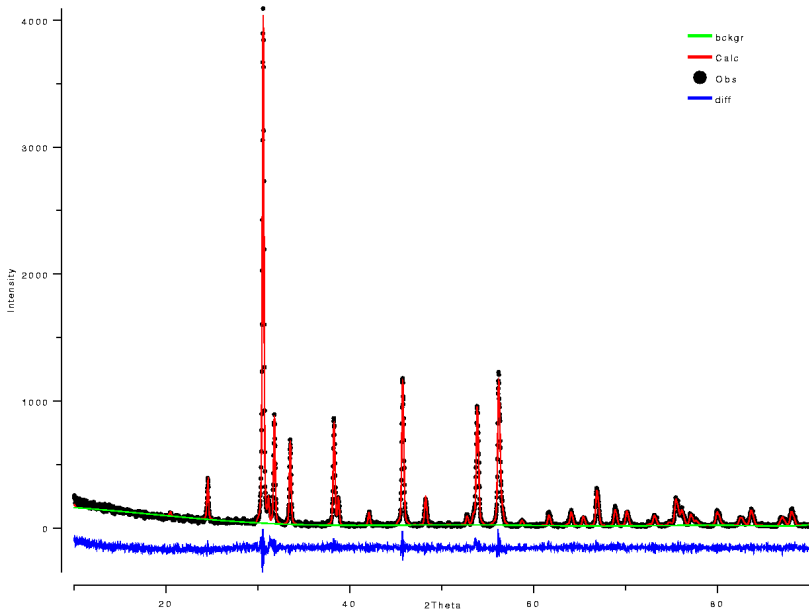


## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$



Temperature-dependent x-ray diffraction (20 sec. pattern)

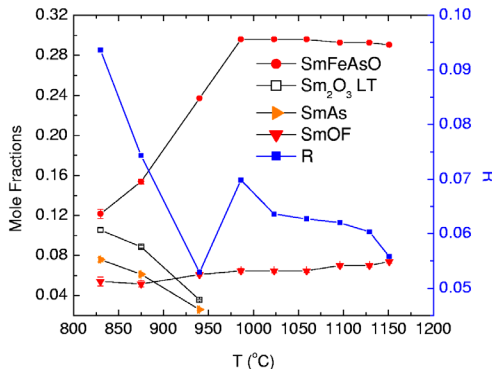
## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$



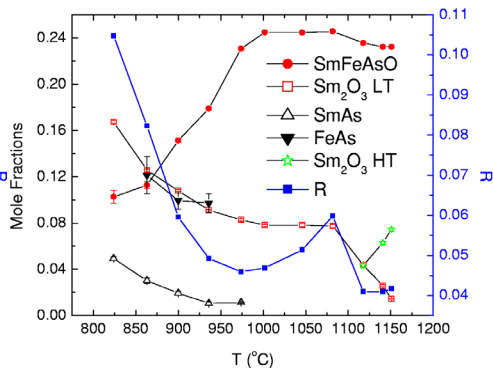
Multi-phase Rietveld refinement

# Example: preparation of $R\text{FeAs}(\text{O/F})$

F doped

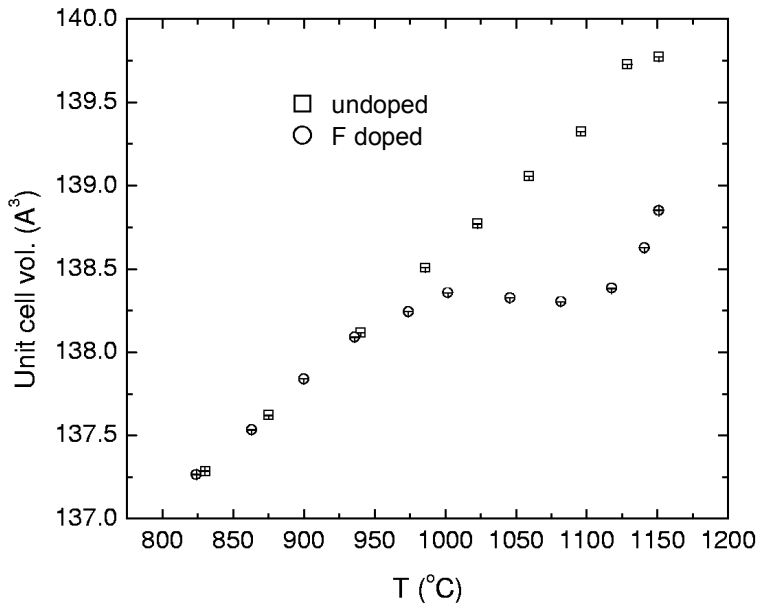


undoped



Crystalline phase fraction determined by Rietveld analysis

## Example: preparation of $R\text{FeAs}(\text{O}/\text{F})$



Unit-cell volume of  $R\text{FeAs}(\text{O}/\text{F})$  phase determined by Rietveld analysis

# Why and when powder for structure determination?

